

# KWISP: an ultra-sensitive force sensor for the Dark Energy sector

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## Abstract

An ultra-sensitive opto-mechanical force sensor has been built and tested in the optics laboratory at INFN Trieste. Its application to experiments in the Dark Energy sector, such as those for Chameleon-type WISPs, is particularly attractive, as it enables a search for their direct coupling to matter. We present here the main characteristics and the absolute force calibration of the KWISP (Kinetic WISP detection) sensor. It is based on a thin  $\text{Si}_3\text{N}_4$  micro-membrane placed inside a Fabry-Perot optical cavity. By monitoring the cavity characteristic frequencies it is possible to detect the tiny membrane displacements caused by an applied force. Far from the mechanical resonant frequency of the membrane, the measured force sensitivity is  $2.0 \cdot 10^{-13} \text{ N}/\sqrt{\text{Hz}}$ , corresponding to a displacement sensitivity of  $1.0 \cdot 10^{-14} \text{ m}/\sqrt{\text{Hz}}$ , while near resonance the sensitivity is  $6.0 \cdot 10^{-14} \text{ N}/\sqrt{\text{Hz}}$ , reaching the estimated thermal limit, or, in terms of displacement,  $3.0 \cdot 10^{-15} \text{ m}/\sqrt{\text{Hz}}$ . These displacement sensitivities are comparable to those that can be achieved by large interferometric gravitational wave detectors.

*Keywords:* Opto-mechanical sensor, Chameleons, Dark Energy, Fabry-Perot

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## 1. Introduction

We have developed an ultra-sensitive opto-mechanical force sensor that can be applied, among other things, to searches for WISP-type particles (Weakly Interacting Slim Particles) able to interact with ordinary matter with a strength  
5 similar to matter-matter interactions. In particular, we intend to shortly use this sensor, called KWISP for "Kinetic WISP detection", to detect the hypothetical flux of Chameleons produced in the sun by exploiting their local density-dependent direct coupling to matter. A flux of solar Chameleons will exert the equivalent of a radiation pressure when impinging at a grazing incidence angle on a solid surface [1, 2]. The KWISP sensor consists of a thin  
10 and rigid dielectric membrane suspended inside a resonant optical Fabry-Perot cavity. The collective force exerted by solar Chameleons bouncing off the membrane surface excites its vibrational states and causes a displacement from its equilibrium position. If a laser beam is frequency-locked to the cavity by means  
15 of an active electro-optical feedback system [3], a membrane displacement from the initial position will cause cavity mode frequencies to experience a shift [4, 5], which is then sensed in the feedback correction signal. The sensor thus transduces displacement (force) into an electrical signal with a gain proportional to the finesse of the Fabry-Perot cavity. Figure 1 shows a pictorial representation  
20 of the KWISP sensor working principle. The displacement sensitivity can be enhanced by exploiting the fact that the membrane is a mechanical resonator with a large figure of merit (Q factor): if an external force acts on it at the resonant frequency, resulting displacements are amplified by Q.

After a description of the sensor itself, we will present measurements done  
25 in the INFN Trieste optics laboratory to characterise it and determine its sensitivity with the direct application of an external force generated by the radiation pressure of an auxiliary laser beam. In the conclusions we will briefly expound

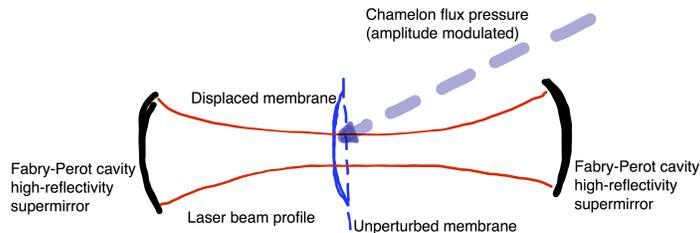


Figure 1: Sketch of the KWISP sensor working principle. The membrane flexes under the action of a time-dependent external force and perturbs the resonance configuration of the intra-cavity electric field (here represented pictorially with an arbitrary beam profile). This in turn causes a shift in the cavity resonant frequencies, which can then be sensed by the feedback keeping laser and cavity in lock (see also text).

on the perspective applications to solar Chameleon searches and to the study of short distance interactions.

## 30 2. The KWISP force sensor

A KWISP force sensor is presently installed in the optics laboratory at INFN Trieste. The main element of the sensor is a vacuum chamber containing an 85 mm long Fabry-Perot cavity made with two 1-inch diameter, 100 cm curvature radius, high-reflectivity, multilayer dielectric mirrors (made by ATFilms, Boulder, Co., USA). The mirror transmission coefficients are  $5.0 \cdot 10^{-5}$  and 0.50 at 1064 nm and 532 nm, respectively. Each mirror is mounted on a two-axis, piezo-actuated, tilting mount (Agilis series by Newport, USA), which is in turn fixed to a common base. A  $\text{Si}_3\text{N}_4$ ,  $5 \times 5 \text{ mm}^2$ , 100 nm thick membrane (made by Norcada Inc., Canada) is inserted in a holder mounted on a 5-axis movement stage, allowing movement of the membrane along 3 linear axes, one of which parallel to the cavity axis, and tilting of it around two additional axes. The reflectivity coefficients for this membrane are 0.10 at 1064 nm, and 0.25 at 532 nm. Using this mechanical assembly, the membrane is initially placed approximately midway between the two cavity mirrors (*membrane-in-the-middle* configuration). Figure 2 shows a photograph of the membrane holder with the (5 mm)x(5 mm)



Figure 2: Photograph of the membrane holder. The  $\text{Si}_3\text{N}_4$  membrane itself is visible as a square-shaped window inside the holder. Membrane dimensions: (5 mm)x(5 mm)x(100 nm).

membrane inside.

The membrane tilting motion is piezo-actuated, similarly to the cavity mirror mounts, and allows one to align the membrane surface parallel to the mirror reflecting surfaces or, equivalently, to align it normal to the cavity axis. Finally, the linear membrane movement along the cavity axis is also piezo actuated (using a piezo chip made by Piezomechanik, Germany) to allow remote positioning of the membrane along the cavity axis with an enhanced nanometer resolution. The cavity-membrane mechanical assembly is visible in the photograph of Figure 3.

The Fabry-Perot cavity is excited using a CW 1064 nm laser beam emitted by a Nd:YAG laser (Prometheus model by Innolight, Germany). This laser is also capable of emitting a second, frequency doubled, CW beam at 532 nm which is used as an auxiliary beam for alignment and for exerting an external pressure on the membrane, as described below. Figure 4 shows a schematic layout of the KWISP sensor optical system.

The layout shown in the figure represents a *two-beam setup*: a 1064 nm

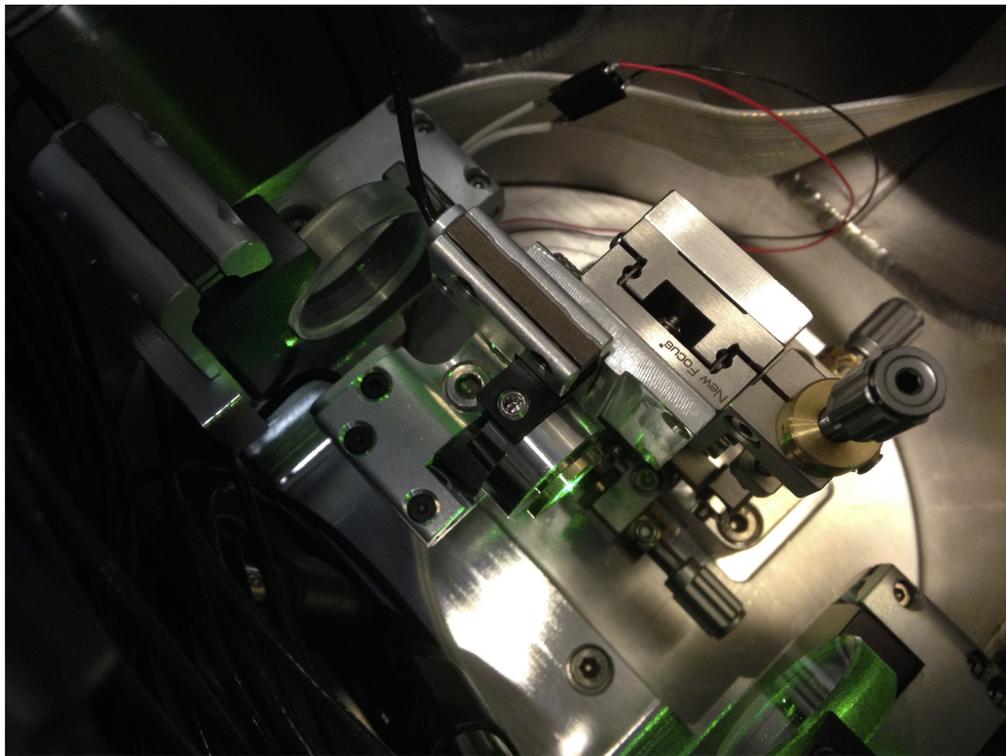


Figure 3: Photograph of the interior of the KWISP sensor vacuum chamber. The membrane holder fixed on its 5-axis mount is visible at center. Cavity mirrors are visible at upper left and lower right. An auxiliary green light beam is used to highlight the main components (see also text).

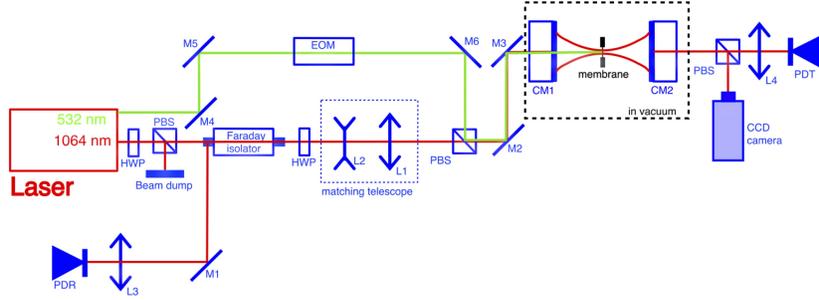


Figure 4: Schematic layout of the KWISP sensor optical system (see text for a detailed description).

*sensing beam* (in red in the figure) and a 532 nm *pump beam* (in green in the figure). The *sensing beam* is kept at resonance with the cavity by means of an electro-optic feedback system [3], and serves to detect membrane displacements.

65 The feedback system (unity gain frequency 60 kHz, [3]) corrects, in different frequency ranges, both for mirror movements and for membrane movements. The measured force sensitivity is, however, not affected, as it is obtained directly from the radiation pressure force exerted by the photons of the pump beam. For the same reason, we do not compensate for possible mirror/membrane relative movements as these are automatically taken into account with the direct force calibration. The *pump beam* is injected in the cavity superimposed on the

70 *sensing beam* and exerts a pressure on the membrane by reflecting off it. Immediately after leaving the laser head, the sensing beam passes through a half-wave plate (HWP) and a polarising beam-splitter (PBS), which allow a controlled attenuation of the beam intensity from a about 800 mW of CW power down to

75 the few mW sufficient for sensor operation. The beam rejected by the PBS is

directed onto a beam dump. After attenuation the beam, which is linearly polarised normal to the optical bench surface, traverses a Faraday isolator having the function of preventing the beam reflected back from the cavity input mirror (CM1) from re-entering the laser cavity and causing instabilities. A second HWP is placed after the Faraday isolator to maximise the intensity transmitted through a second PBS downstream, which allows concurrent injection of the sensing and of the pump beam into the cavity. A matching telescope, consisting of a divergent lens L2 and of a convergent lens L1, has the function of adapting the curvature of the laser beam wavefronts to match the curvature of the cavity mirrors CM1 and CM2, at their respective positions, in order to maximise the light power coupled into the cavity at resonance. The sensing beam is then injected into the Fabry-Perot cavity through a set of steering mirrors (represented by M3 and M4 in the figure). The cavity itself is formed by the two nearly-identical, multi-layer, dielectric mirrors CM1 and CM2. The membrane is also schematically represented in the figure. The nominal cavity finesse was 60000, and without the membrane a finesse of 59000 was actually measured. With the membrane inside the finesse was  $\approx 30000$ . We attribute the difference to losses inside the cavity, mainly scattering from the membrane. We remark here that, however, a finesse measurement is not necessary to obtain the sensitivity thanks to the *pump beam* technique. Light exiting the cavity at resonance passes through a third PBS which further splits it into two beams: one is directed to a CCD camera, used to image the cavity spatial modes for diagnostic and alignment purposes, while the other one is focussed by the convergent lens L4 onto the surface of a photodiode (PDT). The PDT "transmission" photodiode is instrumented with a low-noise, wide-band transimpedance amplifier (Mod. DLPCA-200, by FEMTO, Germany). Light reflected from the cavity propagates backwards through the system up to the Faraday isolator, which steers it to mirror M1, through the convergent lens L3 and onto a second photodiode (PDR, equipped with a Mod. DHPCA-100 transimpedance amplifier by FEMTO, Germany). The back-reflected light intensity is used for diagnostic purposes and also as an input for the electro-optic feedback system keeping the

laser frequency continuously at resonance with the cavity. This system (not represented in Figure 4) is called the Pound-Drever-Hall feedback from its inventors, and is described in [3] and references therein. For the purposes of the present work it sufficient to note that the system works by analyzing the back-reflected beam to obtain a signal proportional to the instantaneous difference between the laser frequency and the cavity frequency. This signal, called the *error signal*, is then amplified and fed back into the laser to control its frequency. The error signal, therefore, contains the information of how the cavity frequency shifts, and it is the signal from which membrane displacement is detected. The 532 nm pump beam is generated inside the laser by frequency duplication of the main 1064 nm beam through a suitable non-linear crystal. This beam is amplitude-modulated by means of an electro-optic crystal excited with a sine signal at a chosen frequency (EOM, mod. 4104 by NewFocus, USA). It is then aligned on top of the main 1064 nm beam by means of a PBS (see Figure 4) and, after passing through the first cavity mirror CM1, reflects off the membrane causing a time dependent force on it. A laser-line filter inserted before the PDR prevents 532 nm light from reaching it. Given a cavity mirror reflectivity of 0.50 at 532 nm, and a slight misalignment with respect to the cavity optical axis, the pump beam does not resonate inside the cavity. The beam waist on the membrane is 260  $\mu\text{m}$  at 1064 nm, and 3.0 mm at 532 nm. With respect to the force sensor the pump beam plays, for instance, the same role that a calibration source plays for a standard radiation detector. Figure 5 shows a photograph of the optical bench hosting the KWISP sensor as seen from the laser head.

### 3. Sensor calibration and sensitivity

During operation the KWISP sensor is in static vacuum with a residual pressure  $< 10^{-3}$  mbar and the whole apparatus is at room temperature. To set the sensor in working mode the Fabry-Perot cavity is frequency locked to the laser. The locking status is monitored by observing on an oscilloscope the control signals from the feedback circuit and the light intensities reflected and

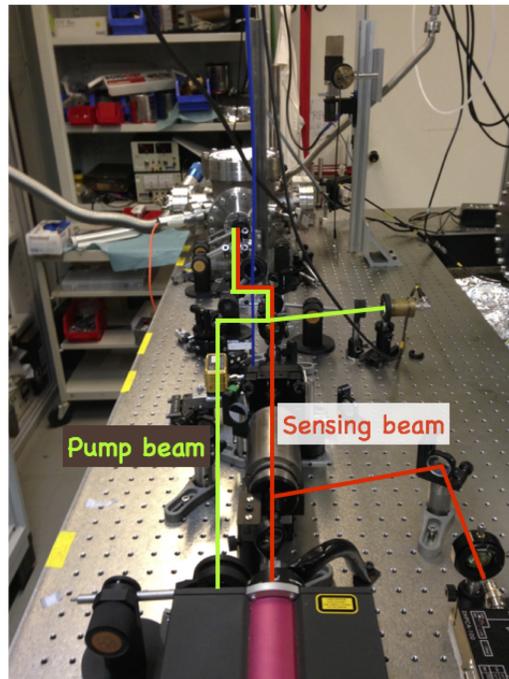


Figure 5: Photograph of the KWISP optical bench as seen from the laser head. The vacuum chamber containing the cavity-membrane assembly is visible at back center. The paths of the two CW beams emitted by the laser are evidenced in the picture. The *sensing beam*, at 1064 nm, is kept at resonance with the cavity by means of a feedback system and serves to detect membrane displacements. The *pump beam*, at 532 nm, is injected in the cavity parallel to the sensing beam and exerts a pressure on the membrane by reflecting off it (see also text).

transmitted by the cavity under lock.

The error signal is proportional to the instantaneous frequency difference between laser and cavity and its power spectrum contains the information on  
140 membrane displacements. To obtain this spectral density, the error signal is fed into an HP35660A Spectrum Analyser, which directly outputs spectral data to a data acquisition computer. In order to achieve an absolute calibration of the sensitivity in terms of force, the pump beam is then injected onto the membrane and amplitude-modulated as described above. The pump light power impinging  
145 on the membrane was  $600 \mu\text{W}$ , and given a measured membrane reflectivity of  $0.25 \pm 0.01$  at  $532 \text{ nm}$ , the light power from the pump beam reflected off the membrane was  $165 \mu\text{W}$ . Taking into account a modulation index of  $0.283$  at  $9.045 \text{ kHz}$ , we find that the maximum amplitude of the light power reflected from the membrane in these conditions is  $47 \mu\text{W}$ , corresponding to a net force  
150 of  $3.1 \cdot 10^{-13} \text{ N}$ . The presence of this force is detected as a peak in the measured spectrum of the error signal. Figure 6 shows the power spectrum of the error signal measured when the pump beam is modulated at  $9.045 \text{ kHz}$ . This value was chosen to fall in a low noise region in the power spectrum of the error signal. The bandwidth of the amplifier-modulator system was also taken into account  
155 in order to achieve maximum depth of modulation with no distortion. The large peak visible in the plot corresponds to the amplitude of the force directly exciting the membrane, while the background is mainly due to electronic noise in the locking circuit. Since the amplitude of the exciting force is independently known, the sensitivity of the sensor can be obtained from the measured signal-to-noise  
160 ratio (SNR). With reference to Figure 6, we find  $\text{SNR} = 10$ , therefore for the chosen integration time of  $40 \text{ s}$ , one has a force sensitivity of  $2.0 \cdot 10^{-13} \text{ N}/\sqrt{\text{Hz}}$ . Recall that this value represents the minimum force amplitude acting on the membrane detectable in  $1 \text{ s}$ .

To illustrate the scaling of the measured background level with the square  
165 root of integration time, Table 1 gives a series of absolute sensitivity measurements done with different integration times.

The membrane is actually a mechanical oscillator, and its behaviour can

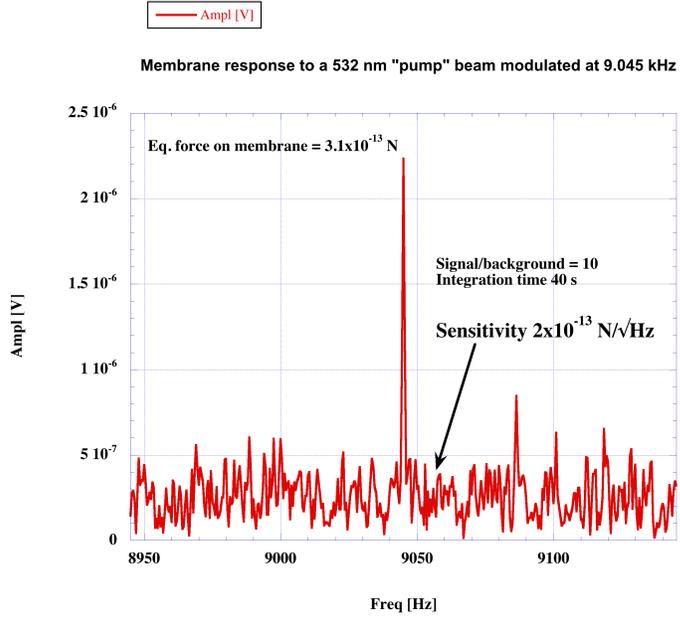


Figure 6: Power spectrum of the cavity feedback error signal when the pump beam is amplitude modulated at 9.045 kHz. The large peak indicates that the membrane is being excited by an external force, while the background is mainly due to electronic noise in the locking circuit. (see text).

Table 1: Background level as a function of integration time measured near the calibration peak

Integration time [s]	Background level [nV]	Sensitivity [fN]
5	560	80
20	316	45
40	180	26

be modelled using a finite element analysis software to obtain its fundamental resonant frequency and its equivalent spring constant. From these simulations  
170 we can assume a spring constant of  $\approx 20$  N/m (this value compares well with the 30 N/m quoted for instance in [6]). Then the equivalent displacement sensitivity of the KWISP sensor is  $1.0 \cdot 10^{-14}$  m/ $\sqrt{\text{Hz}}$  at 9.045 kHz.

The mechanical oscillator behaviour of the membrane and its fundamental resonant frequency can be directly measured with the pump beam technique.  
175 Figure 7 shows the power spectrum of the cavity feedback error signal around 82 kHz when the membrane is excited by a pump beam amplitude-modulated at 9.045 kHz, that is, off the expected fundamental mechanical resonance frequency of the membrane. The red curve in the plot of Figure 7 gives the power spectrum measured when no pump beam is present, showing the presence of a  
180 spurious peak generated in the electronics. The blue curve represents the spectrum measured with the pump beam on, and shows the appearance of a peak at  $\approx 82.5$  kHz. This peak is due to energy from the pump beam coupling to the fundamental mechanical resonant mode of the membrane.

Given the measured fundamental mechanical frequency of the membrane,  
185 one can further investigate the behaviour of the membrane by exciting it with a pump beam amplitude-modulated at frequencies around the mechanical resonant frequency. Preliminary measurements indicate a membrane quality factor of  $Q_{meas} \approx 3000$  and a sensitivity of  $6.0 \cdot 10^{-14}$  N/ $\sqrt{\text{Hz}}$ . The measured Q factor is lower than quality factors in excess of  $10^5$  routinely found in the literature [7, 8]. We attribute our poorer quality factor from these preliminary  
190 measurements to an insufficiently low residual gas pressure in the sensor vacuum chamber, which dampens membrane oscillations. The sensitivity, on the other hand, is near the 300 K thermal limit estimated using the measured Q [6].

#### 4. Conclusions

195 We have built an ultra-sensitive, opto-mechanical force sensor, called KWISP, which is now in operation in the optics laboratory at INFN Trieste. The sensor

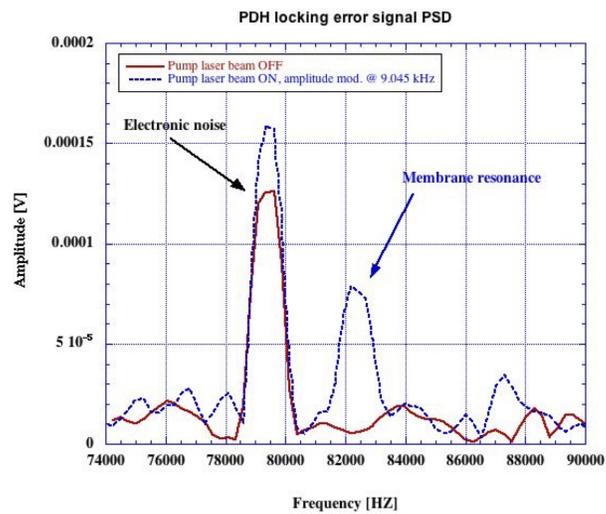


Figure 7: Plot of the power spectrum of the error signal around 82 kHz with the pump beam OFF (red curve) and ON (blue curve). Recall that the pump beam is in this case amplitude-modulated at 9.045 kHz (see also text).

is based on a thin micro-membrane inserted in a Fabry-Perot optical resonant cavity. An absolute calibration of the force sensitivity of this device has been obtained by exciting the membrane with an amplitude modulated light beam.

200 The off-resonance measured force sensitivity is  $3.0 \cdot 10^{-13} \text{ N}/\sqrt{\text{Hz}}$ , corresponding to a sensitivity to membrane displacements of  $1.0 \cdot 10^{-14} \text{ m}/\sqrt{\text{Hz}}$ . Note that this distance is comparable to the average radius of an atomic nucleus. Preliminary measurements around resonance indicate a thermally-limited force sensitivity of  $6.0 \cdot 10^{-14} \text{ N}/\sqrt{\text{Hz}}$ , corresponding to a displacement sensitivity of

205  $3.0 \cdot 10^{-15} \text{ m}/\sqrt{\text{Hz}}$ . This figure is comparable to the displacement sensitivities achieved by large interferometric gravitational wave detectors [9], while our sensor is of course not as sensitive in terms of gravitational waves, given the much shorter length of the Fabry-Perot cavity. For the KWISP sensor under better vacuum it is reasonable to expect  $Q \approx 10^5$  [6], giving a thermally-limited sensitivity of

210  $\approx 2.5 \cdot 10^{-15} \text{ N}/\sqrt{\text{Hz}}$ . A further factor of  $>100$  in sensitivity could be gained by cooling the membrane from room temperature down to sub-K temperatures (30 mK for instance). In this case the projected sensitivity is as low as  $\approx 8.0 \cdot 10^{-18} \text{ N}/\sqrt{\text{Hz}}$ . An immediate application we foresee for the KWISP force-sensor is in the search for Chameleon-type scalar WISPs [2] to be conducted

215 shortly at CAST [10], with the use of the "chameleon chopper" device which we have invented to modulate the flux of solar chameleon, and thus the amplitude of the force by a chameleon beam on the KWISP membrane [11]. There, in CAST, one will exploit both the sun-tracking capability of the moveable magnet carriage, and the presence of an X-ray telescope, which acts also

220 as a focussing device for Chameleons. The extreme sensitivity of the KWISP sensor to tiny displacement makes it also suitable and very attractive for applications in the field of the experimental study of interactions at short distances, with immediate impact on the physics of extra-dimensions and quantum gravity [12, 13, 14, 15].

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