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Aircraft trajectory optimization for weather avoidance and emission reduction applications

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Synthesis

In this thesis are considered two of the biggest problem of the civil aircraft, such as the bad weather avoidance and the fuel consumption and emission reduction, and a possible solution, based on the trajectory optimization, is proposed.

The goal of this work is to propose a method to develop a trajectory optimizer, suitable to run in real time on an on-board device, that provide the pilot with a decision support system, helping him in trajectory optimization for weather avoidance and emission reduction.

In the first part of the thesis the framework is described in terms of European Authorities goals, to reduce aircraft fuel consumption and emissions, and weather phenomenon dangerous for the aircraft flight. An overview of the devices available in aeronautics to detect and predict weather conditions is then provided. In the next chapter an analysis of civil aircraft categories, trajectory, flight phases and flight planning is provided to characterize the object of the optimization (aircraft trajectory). Then different kind of algorithms and method for trajectory optimization are described and compared. In the next chapter our graph based approach for multi-object trajectory optimization is proposed and details about the models used, to generate the graph of feasible trajectories from a certain aircraft in a certain volume of the airspace, are described. Then the results of such a trajectory optimizer applied to real flights in unforeseen weather conditions are provided. Finally, a method to automatically generate the minimum graph of feasible trajectory useful to produce, in real time, an optimized trajectory with a minimum computational time is defined and tested in four use cases.

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CHAPTER 1 INTRODUCTION

The growth experienced by the air transport at a global level in recent years has been translated finally into an increase in the emissions of atmospheric polluting agents, which conflicts with the requirement of reducing the global level of emissions.

The air traffic is expected to triple its size worldwide within 2020, in comparison to year 2000. Huger air traffic means also a greater environmental impact: the increase in number of flights will increase air pollution and level of perceived noise on the ground. Air traffic is estimated to contribute about 3-6% to global warming considering the combined impacts of emissions of CO2, NOx and water vapour. Emission of CO2 and of other air pollutants from air traffic globally is estimated to increase by about 5% per year [5].

From Vision 2020 Report [1] onwards, the Advisory Council for Aeronautics Research in Europe (ACARE) recognized the environment as a major challenge for European Aeronautics and Air Transport, then recommending a total commitment in minimizing the impact on the global environment and confirming this goal in the first edition of the Strategic Research Agenda 1 (SRA-1) [2], in the second updated edition (SRA-2) [3] and in the 2008 Addendum to the Strategic Research Agenda.

As a technological response to such recommendations, the European Commission created the 7th Framework (FP7) Clean Sky Joint Technology Initiative for funding large scale and long term partnerships to implement ambitious and complex activities requiring very huge public and private investments and human resources. Clean Sky, through the validation at a high readiness level, aims at demonstrating the technology breakthroughs necessary to make major steps towards ACARE goals [1,2,3] to be reached in 2020 for the avionic sector.

On the other side weather, especially related to convection, is responsible worldwide for large delays and widespread disruptions especially in the periods of year when travel demand is higher [4]. Weather-induced impacts account for 70% of all delays, with convective weather accounting for 60% of all weather-related delays [5]. Time and location of fast-evolving phenomena like thunderstorms are often very difficult to predict. Because of its unpredictability, weather is the largest contributor to delays over the air traffic control system and is a major factor in aircraft safety incidents and accidents [6].

For the previous motivations, it has been useful to develop a trajectory optimizer, for weather avoidance and emission reduction, based on operational research algorithms, subject of this thesis. In particular, in this thesis is proposed a method to optimize aircraft trajectory for weather avoidance and emission reduction based on Dijkstra algorithm. To better understand the contest, several fields have been taken into account and described here. First of all in this thesis is provided a description of the meteorological models used in aeronautical field and a definition of the dangerous weather condition that can affect the flight. Then an overview of the algorithms for trajectory optimization is provided to have a reference of the methodologies used to solve the same problem that we are considering. Later a description of our trajectory optimization approach and the models used to implement it are provided with some application results. In the following paragraph a method to improve and speed up the trajectory optimization generation is proposed and some results are provided. The proposed approach provides a methodology to optimize trajectory in terms of weather avoidance and emission reduction and provide a solution in a fast and accurate way. Such a problem depends of atmospheric conditions (humidity, pressure, temperature, wind, clouds, ...) and on the airspace in which it is possible to flight that is discretized in a grid of feasible trajectories for a certain aircraft. In fact, in order to compute aircraft emissions, it is required the atmospheric distribution, in altitude, of the following meteorological data: density of air, pressure, temperature, relative humidity, wind intensity, speed and direction, and clouds reflectivity. These data, except density of the air, are available through numerical weather models that several weather organizations in the world develop for analysis of current situations and forecasts.

Moreover, the determination of optimal aircraft trajectories has been of considerable interest to civil aeronautics (ATC, aircraft companies, etc) for almost 50 years. Efforts were put in trying to minimize fuel, time and more recently emissions and noise.

1.1 Thesis Structure

The thesis has the following structure:

- Thanks
- Synthesis
- Content Index

- Figure Index
- Table Index
- Introduction
- Thesis Chapters
- Conclusions
- Bibliography
- Annex

In Section 1 general the scope of this work is summarized. At last an overview of the overall Thesis is given.

In Section 2 is provided an overview of the weather phenomena impacting on trajectory optimization and the main meteorological information required and to be interchanged. Moreover, in this section are also described weather phenomena that can be met during a flight (thunderstorms, lightning, downburst, wind shear, tornado, hail, airframe icing) and it is provided an example of what it is possible to detect, with onboard weather radar, in presence of a cumulonimbus. Finally, an overview of the on board and on ground weather information sources is provided.

In Section 3 is provided an overview civil aircraft categories and a description of the aircraft trajectory, the different phases of flight and trajectory planning.

In Section 4, an overview of different algorithms for trajectory optimization, and a comparison between them, is provided.

In Section 5 our trajectory optimization approach is described as well as the models used to implement it (aircraft BADA model, ICAO model, ISA standard atmospheric model, GRIB weather files, ...)

In Section 6, the results of the trajectory optimizer applied to real scenarios with unforeseen weather events are provided

In Section 7 a method to generate a graph of minimum size, for a selected accuracy is proposed and the calculation results are provided.

In Section 8 the conclusions are provided.

At the end of the thesis are reported the references and acronyms.

CHAPTER 2 WEATHER PHENOMENA OVERVIEW

The weather is the cause of approximately 70 percent of the aircraft delays. In addition, weather continues to play a significant role in a number of aircraft trajectory modification from the preplanned one. The total weather impact is an estimated national cost of \$3 billion for accident damage and injuries, delays, and unexpected operating costs [7].

Unforeseen, adverse weather (other than low visibility and runway condition) and adverse wind conditions (i.e., strong cross winds, tailwind and wind shear) compel the pilot to take sudden decisions regarding trajectory variations with few information, that often are not sufficient to take the right decision in term of emission reduction (for the same safety).

In these cases, at present, for safety reason and luck of information, the pilot manages the event without taking into account aircraft emissions, but only avoidance procedures. In this contest, would be very useful a device able to provide to the pilot more information about alternative safe trajectories taking into account both procedure to avoid the phenomenon and pullant reduction.

2.2 Climatology and interchange of meteorological information

Climatology is important in modern aviation because it studies the phenomenon associate with atmospheric temperature, pressure, precipitation, solar radiation, winds, upper winds and regional climatic environments in different parts of the world, but also particular local meteorological phenomena that affect flying operations [13]. Moreover, climate considers the parameters that mostly influence aircraft performance and emissions, in particular temperature, pressure, humidity, wind and precipitation.

The important aspects of the atmosphere affecting the flight of an aircraft are the location and nature of jet streams, areas of turbulence, location of storm clouds, and the low-level weather for safe landing and take-off. These features of the weather are the result of dynamic and thermal dynamic energy processes within the atmosphere, an understanding of which is essential for the pilot.

On the other side, weather phenomenon are often unpredictable and weather models are not so extremely accurate, so the preplanned trajectories, based on weather prediction, sometimes have to be modified during the flight and update weather condition are required. For this reason, in recent years, weather sensor systems and communication systems for interchange of meteorological information have been improved.

Considering the nature of long haul aviation, pilots need forecasts of the main meteorological phenomena that is required for planning the flight. They also need to understand upper winds, temperatures, tropopause heights, jet streams, mountain waves, thunderstorm activity, tropical cyclones, clear air turbulence (CAT), volcanic activity and such phenomena when conducting the flight. Also, there is the terminal weather (TAFs - Terminal Air Forecasts) and the airports nominated as alternates, both en-route and the destination [15]. Global weather forecasting is becoming a reality. The UK Meteorological Office (MO) is developing its Numerical Weather Prediction (NWP) model, and the resolution of the areas

(grid squares) around the world is improving.

The World Area Forecast Centres (WAFCs) under the provision of ICAO, is centered at two locations, the UK Met Office (Bracknell) and also Washington USA (based in Kansas City). Three INTELSAT 604 satellites provide global coverage. The UK Met Office uses one at 60" E (SADIS Satellite), and covers Europe, the Middle East and South Asia. The USA covers the other half of the globe. The satellites are in geostationary orbit.

The MO produces charts of significant weather from Flight Level 100 to Flight Level 450 for Europe and FL 450 to FL 630 for the North Atlantic. Also spot wind charts for the same areas. Significant weather includes jet streams, heights, direction, and core speeds. The significant weather charts and associated spot winds are produced from FL 250 to FL 450 for the Middle East and South Asia.

Upper wind and temperature charts are produced for ten global regions, twice a day at nine levels. Thus, the total output is 396 charts a day. Only the significant weather charts are combined manually, the rest, E 360, are produced by automation.

The distribution of such charts presently is by the T4 FAX standard of 64 kbit/sec, but a new format to be used is 'GRIB' binary. This is more suitable for transmission of Grid Point

Format charts. The GRIB code is contained in [10,11,15] and the GRIB format will allow world atmosphere models to be transmitted, allowing airlines to optimize their tracks.

The MO increasingly relies on meteorological satellites to provide weather observations particularly over the oceans. Aircraft will provide additional data, but the system will be automated. British Airways will have over 60 aircraft supplying fully automated weather reports. On average, the MO will receive 160 wind and temperature reports daily from each operational aircraft and these are used directly in producing the NWP forecasts, which are becoming the primary method of weather forecasting. This is done by solving a set of equations. A computer model of the atmosphere shows how weather conditions will change over time.

A valuable source of meteorological and climate observations is becoming available from the new Quickscat satellite - on board is NASA's SeaWinds instrument. Access to daily wind data and animations from the ocean-wind tracker are managed by NASA's Jet Propulsion Laboratory (JPL), Pasadena, California.

The heart of SeaWinds is a specially designed spaceborne radar instrument called a scatterometer. The radar operates at a microwave frequency that penetrates clouds. This, coupled with the satellite's polar orbit, makes the wind systems over the entire world's oceans visible on a daily basis. The measurements provide detailed information about ocean winds, waves, currents, polar ice features and other phenomena, for the benefit of meteorologists and climatologists [8,15].

This data will be used operationally by forecasters and for numerical weather prediction models. Upper air observations are also obtained from suitably equipped ships on the Atlantic shipping lanes. This system is presently becoming operational. The MO will receive weather data twice a day for approximately 20 days of each voyage.

Aircraft fitted with the ACARS (Aircraft Communications and Reporting System) Teleprinter system already receive Aircraft Operational Control (AOC), Airline Administrative Control (AAC) and Air Traffic Control (ATC). The system is an air to ground data link system used on HF, INMARSAT, and particularly VHF; however, HF, VHF and UHF frequencies are used. The cockpit equipment consists of a small printer, although, if this fails, a read-out can be seen on the alphanumeric display on the control unit. Through this system, pilots can be alerted to anything unusual which affects the current flight segment. This may include changing weather conditions, updating of TAFs, SIGMETs or mechanical information [8,15]. All these meteorological information, coming from different sources, should be processed, fused and used to improve pilot information and support him in real time during the onboard decisions.

2.3 Weather phenomena impacting on aviation

In the following sub paragraphs are described the weather phenomenon [14] that mostly influence the aircraft performance and require to the pilot a sudden decision in the sense of trajectories modification.

In particular, the following phenomenon are taken into account and described:

- Thunderstorms
- Lightning
- Turbulence (i.e. downburst)
- Wind shear
- Icing
- Hail
- Tornadoes

2.3.1 Thunderstorms

A thunderstorm is a cumulonimbus cloud that contains lightning and thunder. Strong wind gusts, heavy rain, lightning, hail and tornadoes are typical hazards produced by thunderstorms. They usually exist for only a short time, rarely over two hours for a single storm.

The National Weather Service definition of a thunderstorm includes: "accompanied by thunder and lightning" It must produce lightning to be labeled a thunderstorm. It must be electrically active. Lightning is always present, in and near, a thunderstorm.

Thunderstorm development requires three elements:

1) Moisture

2) Lifting Agent

3) Instability

A cumulus cloud forms when moist air is lifted by a thermal, frontal, or orographic process. If the atmosphere is unstable, the lifted air mass will continue to rise and develop into a thunderstorm cell (Fig 1). As the building mass soars upwards, moisture condenses and precipitation-induced downdrafts develop. This process creates violent wind shear and turbulence, and lightning within the cell. Precipitation begins to fall from the cloud base, and the thunderstorm is born.



Fig1 Thunderstorm Development

2.3.1.1 Thunderstorm Stages

The life cycle of a thunderstorm includes three stages: cumulus, mature, and dissipating. Cumulus Stage — is the beginning of all thunderstorms. The size of the updraft region (cell) becomes larger and the cloud grows in an unsteady succession of upward bulges, as evident by the thermals that reach to the top. Strong vertical winds, severe turbulence, icing and lightning, are typical hazards that an aircraft could encounter at this stage.

Mature Stage — is reached when the precipitation-induced downdraft reaches the ground. Heavy rain or hail, and in colder areas sleet or snow, are driven by strong downdrafts. Wind shear, lightning and thunder develop because of friction between the opposing air currents. At this stage, the hazards can be devastating for any aircraft.

Dissipating Stage — is reached when the updraft is overwhelmed by the precipitation induced downdraft. With no source of moisture, the associated hazards decrease and the entire thunderstorm gradually dissipates.

2.3.1.2 Thunderstorm Types

There are several types of thunderstorms: The air mass thunderstorm, the severe thunderstorm, and squall-line thunderstorm. An air mass thunderstorm consists of one cell

and lasts less than one hour, whereas the severe thunderstorm is composed of multi-cells or supercells, and lasts for up to two hours.

2.3.1.3 Air Mass Thunderstorm

The Air Mass Thunderstorm grows quickly and is contained within a single cell. At maturation, the thunderstorm is normally self-destructive. Updrafts elevate water. Water accumulates in the upper areas of the storm. When the upward source can no longer support the accumulated water mass, it rains. The rainfall (downward) overwhelms and strangles the lifting process (upward), and the storm dissipates.

2.3.1.4 Severe Thunderstorm

The Severe Thunderstorm develops when a number of single cells interact and produce more cells (multi cells), thus sustaining the life of the storm.

Specifically, the strong updraft tilts and twists moisture into the upper air support. With strong upper atmosphere winds (for example, the Jet Stream,) the storm tilts or leans downwind. This is evident by the highest portion of the cloud spreading outward (downwind), and forming an anvil shape, fig 32. The water carried upward will accumulate and rain downwind, possibly far ahead of the storm's updraft core. Consequently, the mature stage does not initiate the dissipating stage by strangling the updraft element.

A severe thunderstorm has a greater intensity than an air mass thunderstorm. This is evident by the weather it produces: winds of 50 knots or greater, three-quarters of an inch or larger destructive hail, and/or strong tornadoes.

2.3.1.5 Squall-Line Thunderstorm

Squall line storms are the most disruptive to aviation because they form in lines that can stretch a few hundred miles, and individual storms in the lines can be fierce. Strictly speaking, the lines of storms usually referred to as squall-lines are "pre-frontal squall-lines." Squall lines often trail large areas of stratus clouds with low ceiling and visibility that can linger for hours.



Fig2 Severe Thunderstorm

2.3.1.6 Hazards with thunderstorms

A thunderstorm contains every conceivable aerial hazard: lightning, catastrophic turbulence, wind shear, severe icing, destructive hail, and tornadoes.

2.3.2 Lightning

Lightning is the visible electrical discharge produced by thunderstorms. The convective flow of air currents circulating up and down create friction between the opposing air currents. The friction causes electrical charges within the thunderstorm to separate. Charge separation in the thunderstorm polarizes a region with positive charges at the top, intermediate negative charges within the center, and with positive charges at the base. Since electrical opposites attract, an invisible shadow of negative charges track along the ground beneath the thunderstorm. This is often oversimplified as positive charges at the upper reaches and negative at the base, Fig 3.

Lightning takes place when the positive and negative charge has a voltage difference of about 300,000 volts per foot. Lightning strikes at the speed of light. It may contain up to 200,000 amps of current. With instant air temperature peaks of $50,000^{\circ}$ F along the discharge channel, it is hotter than the sun's surface temperature. The ambient air is exploded into a sonic boom called thunder.

There are three lightning routes: cloud to ground, between the clouds and within the cloud. Most lightning strikes take place within the clouds or between the clouds where aircraft are defenseless targets.



Fig3 Charge Separation

2.3.3 Downburst

Downburst refers to air coming down from a shower or a thunderstorm, hitting the ground, and spreading out. The violent downburst outflow is typically contained within a 3-mile diameter, although velocities beneath thunderstorms have been measured to travel 18 miles in advance of the thunderstorm itself.

2.3.4 Wind Shear

Wind shear is the sudden "tearing" or "shearing" effect when there is a violent change of wind over a short distance. The change can occur in either speed or direction (horizontal and vertical), or both. Wind shear occurs when a concentrated, severe downdraft from within the thunderstorm, known as a downburst, sends an outward burst of very strong damaging winds toward the ground [70,71].

The effect of wind shear on an aircraft can be devastating, especially in low level flight such as taking-off or landing. In these stages of flight the aircraft's performance is severely degraded beyond its capability to compensate.

Wind shear, sometimes referred to as wind shear or wind gradient, is a difference in wind speed and/or direction over a relatively short distance in the atmosphere. Atmospheric wind shear is normally described as either vertical or horizontal wind shear. Vertical wind shear is a change in wind speed or direction with change in altitude. Horizontal wind shear is a change in wind speed with change in lateral position for a given altitude. [14]

Wind shear is a microscale meteorological phenomenon occurring over a very small distance, but it can be associated with mesoscale or synoptic scale weather features such as squall lines and cold fronts. It is commonly observed near microbursts and downbursts caused by thunderstorms, fronts, areas of locally higher low-level winds referred to as low level jets, near mountains, radiation inversions that occur due to clear skies and calm winds, buildings, wind turbines, and sailboats. Wind shear has a significant effect during take-off and landing of aircraft due to its effects on control of the aircraft, and it has been a sole or contributing cause of many aircraft accidents.

Wind shear is sometimes experienced by pedestrians at ground level when walking across a plaza towards a tower block and suddenly encountering a strong wind stream that is flowing around the base of the tower. This phenomenon is a concern for architects.

Sound movement through the atmosphere is affected by wind shear, which can bend the wave front, causing sounds to be heard where they normally would not, or vice versa. Strong vertical wind shear within the troposphere also inhibits tropical cyclone development, but helps to organize individual thunderstorms into longer life cycles which can then produce severe weather. The thermal wind concept explains how differences in wind speed at different heights are dependent on horizontal temperature differences, and explains the existence of the jet stream. [14,15]

2.3.5 Tornado

A Tornado is a swirling column of upward flowing air which is found below cumulonimbus clouds. Wind speeds of up to 180 kts have been recorded. Tornadoes typically have a diameter of 300 feet to 2,000 feet, although there are reported tornadoes of one mile. They occur typically on the south to southwest side of severe thunderstorms in the mid-west. In fact, they occur on the water side, the source of energy.

Storms spawning tornadoes must be given the widest avoidance.

2.3.6 Hail

Hail is precipitation that falls from thunderstorms as round or irregular balls of ice. The freezing process takes place when water droplets are continuously rotated up and down by air currents within the cell of a thunderstorm. Each time a water droplet is pushed by strong updrafts into the cold upper layers, freezing occurs. The process repeats itself until the weight of the hail stone causes it to fall or the updraft subsides enough to allow hail to fall to the ground.

Hail has exited thunderstorms from the long cirrus anvil cloud, many miles distant from the storm center. Hail paths 20 miles down-wind are common.

2.3.7 Airframe Icing

Airframe icing occurs mainly when the aircraft contacts super-cooled water droplets within clouds. Airframe ice seriously degrades the performance and control of any airplane. All thunderstorms contain super cooled water droplets and must be avoided.

2.4 Weather models for aeronautical applications

An atmospheric model is a mathematical model constructed around the full set of primitive dynamical equations which govern atmospheric motions. It can supplement these equations with parameterizations for turbulent diffusion, radiation, moist processes (clouds and precipitation), heat exchange, soil, vegetation, surface water, the kinematic effects of terrain, and convection. Most atmospheric models are numerical, i.e. they discretize equations of motion. They can predict microscale phenomena such as tornadoes, submicroscale turbulent flow over buildings, as well as synoptic and global flows. The horizontal domain of a model is either global, covering the entire Earth, or regional (limited-area), covering only part of the Earth. The different types of models run are thermos-tropic, barotropic, hydrostatic, and non-hydrostatic. Some of the model types make assumptions about the atmosphere which lengthens the time steps used and increases computational speed.

Forecasts are computed using mathematical equations for the physics and dynamics of the atmosphere. These equations are nonlinear and are impossible to solve exactly. Therefore, numerical methods obtain approximate solutions. Different models use different solution methods. Global models often use spectral methods for the horizontal dimensions and finite-difference methods for the vertical dimension, while regional models usually use finite-difference methods in all three dimensions. For specific locations, model output statistics use climate information, output from numerical weather prediction, and current surface weather observations to develop statistical relationships which account for model bias and resolution issues.

There are several numerical weather models available, the main ones are the global version and the regional version [17].

2.4.1 Global versions

Some of the better known global numerical models [13,14,15] are:

- GFS Global Forecast System (previously AVN) developed by NOAA
- NOGAPS developed by the US Navy to compare with the GFS
- GEM Global Environmental Multiscale Model developed by the Meteorological Service of Canada (MSC)
- IFS developed by the European Centre for Medium-Range Weather Forecasts
- UM Unified Model developed by the UK Met Office, but is hand-corrected by professional forecasters
- GME developed by the German Weather Service, DWD, NWP Global model of DWD
- ARPEGE developed by the French Weather Service, Météo-France
- IGCM Intermediate General Circulation Model

2.4.2 Regional versions

Some of the better known regional numerical models are:

WRF The Weather Research and Forecasting model was developed cooperatively by NCEP, NCAR, and the meteorological research community. WRF has several configurations, including:

- WRF-NMM The WRF Non-Hydrostatic Mesoscale Model is the primary short-term weather forecast model for the U.S., replacing the Eta model.
- AR-WRF Advanced Research WRF developed primarily at the U.S. National Center for Atmospheric Research (NCAR)

NAM The term North American Mesoscale model refers to whatever regional model NCEP operates over the North American domain. NCEP began using this designation system in January 2005. Between January 2005 and May 2006, the Eta model used this designation. Beginning in May 2006, NCEP began to use the WRF-NMM as the operational NAM.

RAMS the Regional Atmospheric Modeling System developed at Colorado State University for numerical simulations of atmospheric meteorology and other environmental phenomena on scales from meters to hundreds of kilometers - now supported in the public domain MM5 The Fifth-Generation Penn State/NCAR Mesoscale Model

ARPS the Advanced Region Prediction System developed at the University of Oklahoma is a comprehensive multi-scale non-hydrostatic simulation and prediction system that can be used for regional-scale weather prediction up to the tornado-scale simulation and prediction. Advanced radar data assimilation for thunderstorm prediction is a key part of the system.

HIRLAM High Resolution Limited Area Model

GEM-LAM Global Environmental Multiscale Limited Area Model, the high resolution (2.5 km) GEM by the Meteorological Service of Canada (MSC)

ALADIN The high-resolution limited-area hydrostatic and non-hydrostatic model developed and operated by several European and North African countries under the leadership of Météo-France.

COSMO The COSMO Model, formerly known as LM, aLMo or LAMI, is a limited-area nonhydrostatic model developed within the framework of the Consortium for Small-Scale Modelling (Germany, Switzerland, Italy, Greece, Poland, Romania, and Russia).The COSMO Model (formerly known as LM, aLMo or LAMI) is a limited-area non-hydrostatic model for operational numerical weather prediction, regional climate modelling, environmental prediction (aerosols, pollen and atmospheric chemistry) and research (idealized case studies). A first NWP (Numerical Weather Prediction) version was originally developed by the German Weather Service. It is now further developed by the Consortium for Small-Scale Modelling, the Climate Limited-area Modelling (CLM)-Community, and other research institutes.

2.4.3 GRIB files

The most used meteorological file format is the GRIB (GRIdded Binary or General Regularlydistributed Information in Binary form) from NOAA (National Oceanic and Atmospheric Administration) [11]. The Grib is a concise data format commonly used in meteorology to store historical and forecast weather data. The World Meteorological Organization's Commission for Basic Systems standardize it. Currently there are three versions of GRIB. The first edition (current sub-version is 2) is used operationally worldwide by most meteorological centers, for Numerical Weather Prediction output (NWP). A newer generation has been introduced, known as GRIB second edition, and data is slowly changing over to this format. Some of the second-generation GRIB are used for derived product distributed in Eumetcast of Meteosat Second Generation. Another example is the NAM (North American Mesoscale) model.

GRIB files are a collection of self-contained records of 2D data, and the individual records stand alone as meaningful data, with no references to other records or to an overall schema. Each GRIB record has two components - the part that describes the record (the header), and the actual binary data itself. The data in GRIB-1 are typically converted to integers using scale and offset, and then bit-packed. GRIB-2 also has the possibility of compression.

The most used GRIB files are the Rapid Refresh (RAP) model from NOAA/NCEP operational weather prediction system, running every hour. Such a file contains all the atmospheric conditions required to predict aircraft consumption and emissions.

The RAP is an atmospheric prediction system that consists primarily of a numerical forecast model and an analysis system to initialize the model. Models run hourly, with analysis and hourly forecasts out to 18 hours. RAP files are stored in the GRIB2 file format. The minimum grid spatial resolution is 13 km. In particular, for the tests were used GRIB2 file that uses 37 vertical levels (isobaric levels) with a grid having a horizontal spatial resolution of 20 km with a dimension of 225x301 grid cells. From these files were used geo-referred information about pressure, temperature, relative humidity, wind speed and direction, and clouds reflectivity (from on-ground the weather radar data), the other variable needed were taken from ISA standard model.

2.5 Devices used to detect weather phenomenon

For a pilot situational awareness, the primary source of information about the weather conditions like wind, perturbation, pressure, temperature, humidity, etc. They can be detected on board or on ground with different devices [12,16] that will be described in the following paragraphs.

2.5.1 Onboard information sources

Service aircraft integrate a few number of sensors, commonly used for navigation purposes and to provide environment information to the pilot. The Air Data and Inertial Reference System (ADIRS) calculates flight parameters (Indicated Airspeed, position, etc) directly from probe measurements and supplies with air data a large number of critical aircraft systems (like FMS). The probes network, used for navigation, includes the following sensors:

- Pressure sensors (Pitot probes, Pitot-static probes and static pressure probes)
- Temperature sensors (total air temperature probes)
- Angle of Attack sensors

Figure 1 presents the main location of the previous sensors. For integration purposes, new generation of sensors have been developed. Those multi-function probes (MFP) are able to measure more than one parameters (A380 MFP measure the angle of attack, the total pressure and the temperature).



Fig.4 Example of Probes location in an A380

2.5.1.1 Pressure

Pressure sensors measure various type of pressures, depending on their position and type:

- The static pressure sensor, which measures the static pressure
- The Pitot sensor, which measure the total pressure
- The Pitot-static sensor, which measure both static and total pressure

The statics pressure sensor is used to determine the statics pressure. This information is crucial since, combined with Pitot sensors measurements, it is used to calculates the aircraft velocity (the Indicated Air Speed, which leads to the True Air Speed) and wind speed (combined with inertial data). The number of integrated static pressure sensors varies by manufacturer and aircraft model. Airbus commercial aircrafts are commonly equipped with 6 pressure sensors (3 on each side of the aircraft) while Boeing usually use 3 probes per aircraft. The Pitot sensor provides the aircraft with the total pressure (sum of dynamic pressure and static pressure). The probe is an opened trend tube, parallel with the air flow. The delta between total pressure and static pressure provides the dynamic pressure, required to determine the relative wind speed and the Mach number.

2.5.1.2 Temperature

The total air temperature probes sense total air temperature (TAT), used to calculate the static air temperature (SAT or outer air temperature OAT). The TAT (see Fig. 4) is directly sent to the ADIRS and used (with static and total pressure) to compute the true air speed (TAS). The information is also displayed to the pilot on the electronic flight instrument system (EFIS).

The temperature sensors tolerance is \pm 0.25°C plus 0.5% percent of the magnitude of the temperature in degrees Celsius, with a response time in the air around 1 second.

2.5.1.3 Multi-function probe

The Multi-Function Probe (MFP) combines two or more sensors. This type of probes does not provide any new weather parameter to the aircraft but reduce the number of probes integrated in the fuselage for cost efficiency, and drag reducing purposes. The MFP does not refer to a clear need, and each aircraft and manufacturer integrate different functionalities to the sensor, depending on the aircraft need. The MFP integrated in the A380 and A350 (provided by Goodrich) supply total pressure, total air temperature and angle of attack data (Fig. 5). The static pressure is measure by dedicated probes located on each side of the aircraft. For redundancy purposes, temperature sensors have also been added in the A350 fuselage.



Fig.5 Example of A380 Multi-Function Probes

2.5.1.4 Humidity

Humidity sensors offer real opportunities to improve weather forecast on specific phenomena (clear air turbulence, icing, convection) and provide in-situ measures to evaluate climate changes. Only few aircrafts are already equipped with humidity sensors in Europe but WMO initiative E-AMDAR promotes the integration of hygrometric sensors to improve weather forecast. There are few humidity sensors integrated in European commercial aviation yet but offer a real interest to improve weather forecast. This section will first specify the needs in term of performance and then detail two available humidity sensors integrated in American commercial aviation for AMDAR operating system.

2.5.1.5 Onboard Weather radar

Weather radar is designed to detect precipitation: it helps to identify that associated with the most active convective cells in order to avoid the dangers associated with them (turbulence, hail and lightning).

Weather radar can detect water in liquid form, such as rain and wet hail. However, it hardly detects water in solid form such as dry snow and ice crystals. It can partly detect dry hail depending on the size of the hailstones.

In a convective cell, in the part situated below freezing point (O °C, that mean FL 75 in standard atmosphere), liquid precipitation constitutes the most reflective areas. Below -40°C (at FL 275 in standard atmosphere) water no longer exists in general in a liquid state. In the part of the cumulonimbus between freezing point and the altitude where the temperature

reaches -40 °C, liquid water and ice crystals produce areas where reflectivity decreases depending on the variation of the presence of liquid water. In the part above the altitude where the temperature reaches -40 °C, where there are only ice crystals, reflectivity is very low.

Areas returning most of the radar signal may be harmless for flight, like melted snow showers for example, whereas hail showers which constitute a genuine threat to navigation may only return a weak radar echo.

When cumulonimbus clouds swell swiftly, they may be overtaken by a zone of severe turbulence which could stretch several thousand feet above the visible peak. This turbulence zone is invisible to weather radar and the naked eye (The TURB function, which uses the principle of the Doppler effect, only helps detection of turbulence in wet zones).



Fig.6 Anatomy of a cumulonimbus

The representation of the same cumulonimbus cloud will therefore be totally different depending on the part of the cloud that is scanned by the radar beam.

Cloud mass reflectivity depends on the type of air mass and on the season. Cumulonimbus reflectivity is not the same in temperate regions and below the equator. An oceanic cumulonimbus reflects radar waves less than a continental cumulonimbus cloud of the same size and height.
Gain, tilt and the ND scale enable pilots to adjust the weather radar. Gain defines the level ratio between the signal received and the signal emitted according to the distance of the echoes. The CAL position of the gain control sets radar sensitivity at the standard calibrated level of reflectivity. The equivalence in precipitation is thus associated with a colour of the echoes presented on the ND:

COULEUR DES ECHOS	NIVEAU	EQUIVALENCE EN PRECIPITATIONS
NOIR (pas d'écho)	1	< 1 mm/H
VERT	2	1 à 4 mm/H
JAUNE	3	4 à 12 mm/H
ROUGE	4	>12 mm/H
MAGENTA (si installé)	TURB	Effet Doppler

Table 1 Extract from Air France A330/340 operations manual

The gain control allows the manual adjustment of radar sensitivity for a more precise evaluation of atmospheric conditions.

Tilt is the angle between the horizontal and the center of the radar beam. The tilt control enables the range explored in the vertical plane to be varied manually. Depending on the altitude of the aircraft, at a specific tilt, the radar beam is reflected by the ground. Ground echoes are then present on the radar image.

Adjusting the ND scale enables monitoring at varying distances of the aircraft.

Heavy precipitation that returns most of the radar signal may also hide another disturbed area situated behind.

Representation of the weather situation by crews is thus mainly linked to the use of the 3 setting parameters and their knowledge of radar, particularly of its limitations.

Onboard radar does not directly detect dangers to be avoided and has specific limitations which require active monitoring from the pilots and constant analysis of the images presented to limit the risk of underestimating the danger of the situation. It should be noted that, at the time of the accident, the presence of ice crystals at high altitude was not considered to be an objective danger and that crews were not made aware of this.

2.5.2 On ground information sources

The weather information is also collected on-ground by several kinds of devices and provided to the pilot through the ATC (Aircraft Traffic Control) by different types of messages taken into account in the next paragraph. The main on-ground weather data sources are:

- On-ground weather radar
- Meteorological stations
- On-ground meteorological predictions

The on-ground weather radar has the same behavior of the on-board weather data, the meteorological stations are composed by different sensors, similar to the on-board sensors. The meteorological predictions are based on the meteorological models described in the previous paragraphs.

CHAPTER 3 OVERVIEW ON CIVIL AIRCRAFT FLIGHT

Aircraft can be divided in 3 main weight categories that have a different behavior respect the weather condition and trajectory. In this chapter are described and characterized the 3 aircraft categories, the phase of flight in which the aircraft trajectory can be divided and an overview of the trajectory optimization methods is provided.

3.1 Aircraft categories

The ICAO wake turbulence category (WTC) is entered in the appropriate single character wake turbulence category indicator in Item 9 of the ICAO model flight plan form and is based on the maximum certificated take-off mass, as follows [13]:

- H (Heavy) aircraft types of 136 000 kg (300 000 lb) or more (i.e. long range aircraft like A320);
- M (Medium) aircraft types less than 136 000 kg (300 000 lb) and more than 7 000 kg (15 500 lb) (i.e. regional aircraft like ATR72); and
- L (Light) aircraft types of 7 000 kg (15 500 lb) or less (i.e. ultra-light aircraft like Cessna)

Variants of an aircraft type may fall into different wake turbulence categories, (e.g. L/M or M/H). In these cases, it is the responsibility of the pilot or operator to enter the appropriate wake turbulence category indicator in the flight plan.

3.2 Phase of flight

The aircraft movement can be divided in 6 main phases characterized by different speed, altitude and aircraft attitude:

- taxing
- Take-off
- Climb
- Cruise
- Descent
- Landing



Fig.7 representation of aircraft trajectory with the different phases of flight

3.2.1 Taxing

Taxiing refers to the movement of an aircraft on the ground, under its own power. The aircraft moves on wheels. An airplane uses taxiways to taxi from one place on an airport to another; for example, when moving from a terminal to the runway.

The aircraft always moves on the ground following the yellow lines, to avoid any collision with the surrounding buildings, vehicles, or other aircrafts. The taxiing motion has a speed limit. Before making a turn, the pilot reduces the speed further to prevent tire skids. Just like cars, there is a certain list of priorities during taxiing. The aircrafts that are landing or taking off have higher priority. The other aircrafts must wait for these aircrafts before they start or continue taxiing.

The thrust to propel the aircraft forward comes from its propellers or jet engines. Steering is achieved by turning a nose wheel or tail wheel/rudder; the pilot controlling the direction travelled with their feet. The use of engine thrust near terminals is restricted due to the possibility of jet blast damage. Therefore, the aircrafts are pushed back from the buildings by a vehicle before they can start their own engines for taxiing.



Fig.8 aircraft phases of flight and emissions target to be reduced

3.2.2 Take-off

Takeoff is the phase of flight in which an aircraft goes through a transition from moving along the ground (taxiing) to flying in the air, usually starting on a runway. Usually the engines are run at full power during takeoff. Following the taxi motion, the aircraft stops at the starting line of the runway. Before takeoff, the engines, particularly piston engines, are routinely run up at high power to check for engine-related problems. This makes a considerable noise. When the pilot releases the brakes, the aircraft starts accelerating rapidly until the necessary speed for take-off is achieved.

The takeoff speed required varies with air density, aircraft weight, and aircraft configuration (flap and/or slat position, as applicable). Air density is affected by factors such as field elevation and air temperature.

The speeds needed for takeoff are relative to the motion of the air (indicated airspeed). A head wind will reduce the ground speed needed for takeoff, as there is a greater flow of air over the wings. This is why the aircraft generally take off against the wind. Side wind is not preferred as it would disturb the stability of the aircraft. Typical takeoff air speeds for jetliners are in the 130–155 knot range (150–180 mph, 240–285 km/h). For a given aircraft, the takeoff speed is usually directly proportional to the aircraft weight; the heavier the weight, the greater the speed needed. Some aircraft have difficulty generating enough lift at the low speeds encountered during takeoff. These are therefore fitted with high lift devices, often including slats and usually flaps, which increase the camber of the wing, making it more effective at low speed, thus creating more lift. These have to be deployed from the wing before performing any maneuver.

At the beginning of the climb phase, the wheels are retracted into the aircraft and the undercarriage doors are closed. This operation is audible by the passengers as a noise coming from below the floor.

3.2.3 Climb

Following take-off, the aircraft has to climb to a certain altitude (typically 30,000 ft or 10 km) before it can cruise at this altitude in a safe and economic way. A climb is carried out by increasing the lift of wings supporting the aircraft until their lifting force exceeds the weight of the aircraft. Once this occurs, the aircraft will climb to a higher altitude until the lifting force and weight are again in balance. The increase in lift may be accomplished by increasing the angle of attack of the wings, by increasing the thrust of the engines to increase speed (thereby increasing lift), by increasing the surface area or shape of the wing to produce greater lift, or by some combination of these techniques. In most cases, engine thrust and angle of attack are simultaneously increased to produce a climb.

Because lift diminishes with decreasing air density, a climb, once initiated, will end by itself when the diminishing lift with increasing altitude drops to a point that equals the weight of the aircraft. At that point, the aircraft will return to level flight at a constant altitude. During climb phase, it is normal that the engine noise diminishes. This is because the engines are operated at a lower power level after the take-off. It is also possible to hear a whirring noise or a change in the tone of the noise during climb. This is the sound of the flaps that are retracting. A wing with retracted flap produces less noise.

3.2.4 Cruise

Cruise is the level portion of aircraft travel where flight is most fuel efficient. It occurs between ascent and descent phases and is usually the majority of a journey. Technically, cruising consists in a flight with constant airspeed and altitude. It ends as the aircraft approaches the destination where the descent phase of flight commences in preparation for landing.

For most commercial passenger aircraft, the cruise phase of flight consumes the majority of fuel. As this lightens the aircraft considerably, higher altitudes are more efficient for additional fuel economy. However, for operational and air traffic control reasons it is necessary to stay at the cleared flight level. Typical cruising speed for long-distance commercial passenger flights is 475-500 knots (878-926 km/h; 547-578 mph).

Commercial or passenger aircraft are usually designed for optimum performance at their cruise speed. There is also an optimum cruise altitude for a particular aircraft type and conditions including payload weight, center of gravity, air temperature, humidity, and speed. This altitude is usually where the drag is minimum and the lift is maximum. As in any phase of the flight, the aircraft in cruise mode is always in communication with an Air Traffic Control (ATC) station. Although the general tendency is to follow a straight line towards the destination, there may be some deviations from the flight plan for weather, turbulence or air traffic rea- sons, after receiving clearance from ATC.

3.2.5 Descent

A descent during air travel is any portion where an aircraft decreases altitude. Descents are an essential component of an approach to landing. Other partial descents might be to avoid traffic, poor flight conditions (turbulence or bad weather), clouds (particularly under visual flight rules), to see something lower, to enter warmer air (in the case of extreme cold), or to take advantage of wind direction of a different altitude. Normal descents take place at a constant airspeed and constant angle of descent (3-degree final approach at most airports). The pilot controls the angle of descent by varying engine power and pitch angle (lowering the nose) to keep the airspeed constant.

A peculiar flight technique is applied from Pilot to save fuel and obtain noise abatement during descent. This technique is based on a computation of the "top of descent point", a point where, if no diversion (traffic or weather) occurs, engines power will be reduced and never increase till landing phase. In other words, the achievement is a continue descent to the destination airport whiteout any interruption of level flight phase such required an increase of engine power, fuel consumption and noise.

At the beginning of and during the descent phase, the engine noise diminishes further as the engines are operated at low power settings. However, towards the end of the descent phase, the passenger can feel further accelerations and an increase in the noise. This is to realize the "final approach" before taking "landing position".

3.2.6 Landing

Landing is the last part of a flight, where the aircraft returns to the ground. Aircraft usually land at an airport on a firm runway, generally constructed of asphalt concrete, concrete, gravel or grass. To land, the airspeed and the rate of descent are reduced to where the object descends at a slow enough rate to allow for a gentle touch down. Landing is accomplished by slowing down and descending to the runway. This speed reduction is accomplished by reducing thrust and/or inducing a greater amount of drag using flaps, landing gear or speed brakes. As the plane approaches the ground, the pilot will execute a flare (round out) to induce a gentle landing. Although the pilots are trained to perform the landing operation, there are "Instrument Landing Systems" in most of the airports to help pilots land the aircraft. An instrument landing system (ILS) is a ground-based instrument approach system that provides precision guidance to an aircraft approaching and landing on a runway, using a combination of radio signals and, in many cases, high-intensity lighting arrays to enable a safe landing during instrument meteorological conditions (IMC), such as low ceilings or reduced visibility due to fog, rain, or blowing snow.

At the beginning of the landing phase, the passengers will hear the opening of the doors of the landing gears. As the landing gears are deployed, they will create an additional drag and an additional noise. Immediately after touch-down, the passengers can hear a blowing sound, sometimes with increasing engine sound. This is the engine's thrust reverses, helping the aircraft to slow down to taxi speeds by redirecting the airflow of the engines for- ward. Is a way to decelerate without overload the landing gear braking system. This phase is the noisiest of landing. Once the aircraft is decelerated to low speed, it can taxi to the terminal building.

3.3 Flight Planning

The process of producing a flight plan to describe the trajectory of a proposed flight is called flight planning. It basically involves coming with an estimate of amount of fuel required for the flight and the trajectory of flight, describing the route to be taken to reach the destination safely, which complies with the air traffic control procedures/regulations. Civil airlines would wish to plan the trajectory in such a way that it would minimize a certain cost index.

The procedure of coming up with a flight plan is highly dependent on a lot of factors and is very problem specific. It depends on specific origin-destination pair, type of aircraft being used and weather forecast. Flight planning requires accurate weather forecasts so that fuel consumption calculations can account for the fuel consumption effects of head or tail winds and air temperature. Producing an optimal flight plan even for a given origin-destination pair, a specific aircraft and initial weight, is never a one-time process. The air temperature aspects the efficiency/fuel consumption of

aircraft engines. The wind may provide a head or tail wind component which in turn will increase or decrease the fuel consumption by increasing or decreasing the air distance to be own. Hence, accurately updated weather forecast plays a crucial role in coming up with an optimal trajectory.

Furthermore, it is required as per safety procedures to carry fuel beyond the minimum needed to y to the specified destination. Under the supervision of air traffic control, aircraft flying in controlled airspace must follow predetermined routes known as airways, even if such routes are not as economical as a more direct flight.

Within these airways, aircraft must maintain flight levels, specified altitudes usually separated vertically by 1000 or 2000 feet, depending on the route being own and the direction of travel. When aircraft with only two engines are flying long distances across oceans, deserts, or other areas with no airports, they have to satisfy extra safety rules to ensure that such aircraft can reach some emergency airport if one engine fails. Rate of fuel burn depends on ambient temperature, aircraft speed, and aircraft altitude, none of which are entirely predictable. Rate of fuel burn also depends on airplane weight, which changes as fuel is burned.

Coming up with an accurate optimized flight plan for commercial airlines is by itself a big industry. Producing an accurate optimized flight plan requires a large number of calculations (millions), so commercial flight planning systems make extensive use of computers. Some commercial airlines have their own internal flight planning system, while others employ the services of external planners. While developing a software tool to plan flight trajectory, it is necessary to incorporate commercial flight procedures followed. They add in a lot more constraints to the flight path. These are discussed in the following section.

3.3.1 Commercial flight procedures

In a realistic civil aircraft flight, the complete trajectory is broken into series of flight segments, mainly broken into phases as shown in Fig. 9. Each of these phases in turn include several flight segments, where each segment can be defined by control objectives and termination conditions designed to be flyable. Mathematically, each flight segment can be described by two constant control variables selected from among engine thrust setting, Mach number or calibrated airspeed, and altitude rate or flight path angle [18].



Fig.9 Complete trajectory for an aircraft from takeoff to landing

Furthermore, airline specifications often combine a number of segments in a specified order to form certain profiles. A lateral profile can be defined for an aircraft flying level and turning at constant bank angle using waypoints.

Aircraft takeoff and descent is divided into a sequence of segments defining a vertical profile. Each vertical flight segment is defined by choosing exactly two control objectives, at most one from each category. This either explicitly or implicitly defines how the aircraft pitch and thrust are controlled. For example, choosing constant Mach and idle thrust defines a descent segment that control speed using aircraft pitch.

3.3.1.1 Lateral profile

Lateral profile of a flight usually describes the level flight portion. The aircraft makes turns at a constant bank angle. A lateral profile is usually described by a sequence of waypoints (Area Navigation (RNAV)). Most waypoints are classified as compulsory reporting points, i.e. the pilot (or the onboard flight management system) reports the aircraft position to air traffic control as the aircraft passes a waypoint. There are two main types of waypoints. A named waypoint appears on aviation charts with a known latitude and longitude. Such waypoints over land often have an associated radio beacon so that pilots can more easily check where they are. Useful named waypoints are always on one or more airways. A geographic waypoint is a temporary position used in a flight plan, usually in an area where there are no named waypoints, e.g. most oceans in the southern hemisphere. Air traffic control require that geographic waypoints have latitudes and longitudes which are a whole number of degrees.

3.3.1.2 Vertical profile - SID & STAR

After take-off, an aircraft follows a Departure Procedure (SID or Standard Instrument Departure) which defines a pathway from an airport runway to a waypoint on an airway, so that an aircraft can join the airway system in a controlled manner. Most of the climb portion of a flight will take place on the SID. Although a SID will keep aircraft away from terrain, it is optimized for ATC route of flight and will not always provide the lowest climb gradient. It strikes a balance between terrain and obstacle avoidance, noise abatement (if necessary) and airspace management considerations. Before landing an aircraft follows an Arrival Procedure (STAR or Standard Terminal Arrival Route) which defines a pathway from a waypoint on an airway to an

airport runway, so that aircraft can leave the airway system in a controlled manner.

STAR usually covers the phase of a flight that lies between the top of descent from cruise or en-route flight and the final approach to a runway for landing. Normally that final approach starts at the so-called Initial Approach Fix (IAF). A typical STAR consists of a set of starting points, called transitions, and a description of routes (typically via waypoints) from each of these transitions to a point close to destination airport.



Fig.10 Descent profile for a commercial aircraft

There the aircraft can join an instrument approach (IAP) or will be vectored for a final approach by the APP control. Not all airports have published STARs. However, most relatively large or not easily accessible (for example, in the mountainous area) airports do. Sometimes several airports in the same area share a single STAR; in such case, aircraft destined for any of the airports in such group follow the same arrival route up until reaching the final waypoint, after which they join approaches for their respective destination airports.

CHAPTER 4 OVERVIEW ON ALGORITHMS FOR TRAJECTORY OPTIMIZATION

4.1 Review of the Literature

Proposed in 1931, the Zermelo's Navigation Problem was the first posed optimal control problem posed [33]. The problem was to find an optimal path for a boat navigating in a water body in presence of water currents and wind. Without considering any current or wind or any such external force, the optimal control is to follow a straight-line segment from origin to destination. But otherwise, the optimal path is in general never the line joining origin and destination. The same problem was formulated for an aircraft and calculus of variation approach was used to solve it assuming a at earth. Bryson and Ho. later developed a solution technique called neighboring optimal control (NOC) to come up with a solution for Zermelo's problem [34]. The technique of neighboring optimal control (NOC) produces time-varying feedback control that minimizes a performance index to second order for perturbations from a nominal optimal path. This technique was later extended to handle cases of parameter change in the system dynamic model [35]. This extension is used to develop an algorithm for optimizing horizontal aircraft trajectories in general wind fields using time-varying linear feedback gains. The minimum-time problem for an airplane traveling horizontally between two points in a variable wind field (a type of Zermelo problem) was used to illustrate the

above technique. The NOC solution was derived analytically for the case where the wind field was modeled as a constant wind Jardin and Bryson further extended the neighboring optimal control (NOC) technique for computing minimum-time paths through general wind fields by modeling winds along a nominally straight-line path as additional system states [36]. This advancement, referred to as Neighboring Optimal Wind Routing (NOWR), allowed the neighboring optimal control gain solution to be parameterized for different wind conditions and different origin/destination pairs. The winds were modeled at an arbitrary number of discrete points along the nominal great-circle route so that gains are computed for the wind perturbations at each point. Gains are computed once offline and then applied to a wide variety of trajectories between different locations at different altitudes and at different flight speeds. Jardin further demonstrated how to apply the solution to flights on the sphere through coordinate rotations and normalizations and presented analytical solutions for the neighboring optimal gains. In 2010, Jardin and Bryson described two methods to solve a minimum time flight path at high altitude in presence of strong horizontal winds [37]. The first method was using nonlinear feedback (dynamic programming) solutions for minimumtime flight paths. A Zermelo Problem for arbitrary winds was extended from a at earth model to a spherical earth model as a two-state problem (latitude and longitude) with one control (heading angle). The second method is based on an analytical neighboring optimal control solution that computes neighboring optimal heading commands as a function of the winds along a nominal flight path.

Most of the work mentioned above deals with the cruise portion of the flight.

Some of them even assume constant speed throughout the flight. The cruise flight being the major portion of a flight, this has indeed been research topic with most of the works done in flight trajectory optimization, beginning with a series of thesiss by Zagalsky et al.,[38] Schultz and Zagalsky [39], Speyer [40] and [41], and Schultz [42].

In Ref. [38] the authors examined the long-range optimal aircraft cruise problem with the energy-range model. Speyer in 1976 [41] proved using second-order variational analysis and a frequency-domain version of the classical Jacobi (conjugate point) optimality condition that the steady-state cruise for a long-time span is non-optimal with respect to fuel economy. In 1989 P.K. Menon [43] analyzed the long-range cruise problem using point mass and an energy model and showed that the steady state cruise exists as central member along with several other oscillatory extremals. There has been a constant mention in the literature about fuel efficiency of periodic flights - [44], [45] and [46].

Although not as significant as the cruise portion, the climb and the descent portion of the flight has also been studied and optimal strategies were proposed. In 1975, A. Chakravarty in 1983 introduced the concept of an optimal cruise descent [47]. Optimal results were compared with the conventional strategies of constant Mach, Vcas and flight path angle descent segments. The effects of wind on cost of delay was also discussed. In [48],

representative minimum-fuel flight paths of various types are computed for a commercial jet transport close to the terminal area. [49] studies the characteristics of optimum fixed-range trajectories whose structure is constrained to climb, steady cruise, and descent segments by using optimal control theory.

In 2002, Clarke et al. designed and flight-tested a Continuous Descent Approach (CDA or also known as OPD - optimized descent approach) procedure for UPS operated Boeing B767-300 aircraft at the end of the nightly UPS arrival bank at Louisville International Airport [23]. This was mainly designed as a noise abatement procedure and it was shown to reduce the A-weighted peak noise level at seven locations along the flight path by 3.9 to 6.5 dBA. The CDA procedure was also shown to reduce the flight time in the terminal area of the Boeing B767-300 aircraft used in the test by up to 100 seconds relative to the nominal approach procedure, and the corresponding fuel burn by up to 500 pounds [50]. However, widespread implementation of CDA has been limited by the capabilities of both air traffic controllers and air traffic control (ATC) automation. Because it is difficult to predict the future position of an aircraft when its speed varies significantly, air traffic controllers typically instruct all aircraft to y a staged approach, where at each stage the aircraft maintain a common altitude and speed. A lot of variations of CDA have also been studied. A tailored arrival was designed to accommodate CDA under constrained airspace [51]. A tailored arrival creates a fourdimensional continuous descent from cruise altitude to the runway. Demonstrations of oceanic arrivals at San Francisco (SFO) have successfully demonstrated significant fuel savings. Since 2002, significant

research has gone into studying practical implementations of CDA, its variations and comparisons with current procedures and its efficiency - [52], [53], [54], [55], [56] and [57]. Most trajectory optimization schemes use calculus of variation or optimal control theory which are continuous time methods. Discrete methods were also used as early as 1950's. Dixon Speas formed a small company to serve clients in the airline industry. One of his services was to plan minimum-time paths for flights over the Atlantic Ocean. His engineers used discrete dynamic programming, dividing the path into 15 to 20 regions and using high altitude wind data from weather balloons. In the 1970s, Lou Reinkins at Lockheed started a flight planning service for airlines and private aircraft for flights in the United States. Starting in the 1980s, Jeppesen JetPlan did

the same thing for the airlines and private pilots and included international flights.

Due to large runtime and memory management issues, discrete search strategies have seldom been used to plan aircraft trajectories. Discrete algorithms have mainly been used in robotics and UAV path planning in presence of obstacles. In [58], Sellier discusses the use of discrete search methods for real time flight path optimization. It also presents discrepancies and inefficiencies of the cost index concept which is still currently in use in the most advanced flight management systems. Mixed integer linear programs have also been used to

solve for real time trajectory planning for UAV's [59] and for trajectory planning with collision avoidance [60]. Iris Yang and Yiyuan in [61] present a discrete search strategy potential real-time generations of four-dimensional trajectories for a single autonomous aerospace vehicle amid known obstacles and conflicts.

There are surplus examples to show the popularity of use of discrete methods like Dijkstra's algorithm or dynamic programming in the context of UAV's. But they have rarely been used to plan commercial aircraft trajectories. In this work, we plan to show the effectiveness and flexibility of A* algorithm in incorporating the large number of trajectory constraints placed on a commercial aircraft by the air traffic regulations.

4.2 Algorithms for trajectory optimization

Trajectory optimization is the process of designing a trajectory that minimizes (or maximizes) some measure of performance while satisfying a set of constraints. Generally speaking, trajectory optimization is a technique for computing an open-loop solution to an optimal control problem. It is often used for systems where computing the full closed-loop solution is either impossible or impractical.

Although the idea of trajectory optimization has been around for hundreds of years (calculus of variations, brachystochrone problem), it only became practical for real-world problems with the advent of the computer. Many of the original applications of trajectory optimization were in the aerospace industry, computing rocket and missile launch trajectories. More recently, trajectory optimization has also been used in a wide variety of industrial process and robotics applications.

The main typologies of optimization algorithms that we can identify are:

- Direct methods
- Indirect methods
- Shooting methods
- Collocation methods
- Mesh

In the following paragraphs, we will provide a description of a set of these algorithms.

4.2.1 The typical terminology for trajectory optimization

For sake of simplicity here are reported some definitions, related to the algorithms, that will be used later.

Decision variables is the set of unknowns to be found using optimization.

Trajectory optimization problem is a special type of optimization problem where the decision variables are functions, rather than real numbers.

Parameter optimization-Any optimization problem where the decision variables are real numbers.

Nonlinear program-A class of constrained parameter optimization where either the objective function or constraints are nonlinear.

Indirect method-An indirect method for solving a trajectory optimization problem proceeds in three steps: 1) Analytically construct the necessary and sufficient conditions for optimality, 2) Discretize these conditions, constructing a constrained parameter optimization problem, 3) Solve that optimization problem [62].

Direct method-A direct method for solving a trajectory optimization problem consists of two steps: 1) Discretize the trajectory optimization problem directly, converting it into a constrained parameter optimization problem, 2) Solve that optimization problem.[62]

Transcription-The process by which a trajectory optimization problem is converted into a parameter optimization problem. This is sometimes referred to as discretization. Transcription methods generally fall into two categories: shooting methods and collocation methods.

Shooting method-A transcription method that is based on simulation, typically using explicit Runge-Kutta schemes.

Collocation method (Simultaneous Method)-A transcription method that is based on function approximation, typically using implicit Runge--Kutta schemes.

Pseudospectral method (Global Collocation)-A transcription method that represents the entire trajectory as a single high-order orthogonal polynomial.

Mesh (Grid)-After transcription, the formerly continuous trajectory is now represented by a discrete set of points, known as mesh points or grid points.

Mesh refinement-The process by which the discretization mesh is improved by solving a sequence of trajectory optimization problems. Mesh refinement is either performed by subdividing a trajectory segment or by increasing the order of the polynomial representing that segment.[63]

Multi-phase trajectory optimization problem-Trajectory optimization over a system with hybrid dynamics can be achieved by posing it as a multi-phase trajectory optimization problem. This is done by composing a sequence of standard trajectory optimization problems that are connected using constraints.[64]

4.2.2 Trajectory optimization techniques

The techniques to any optimization problems can be divided into two categories: indirect and direct. An indirect method works by analytically constructing the necessary and sufficient conditions for optimality, which are then solved numerically. A direct method attempts a direct numerical solution by constructing a sequence of continually improving approximations to the optimal solution [62]. Direct and indirect methods can be blended by an application of the convector mapping principle of Ross and Fahroo [65].

The optimal control problem is an infinite-dimensional optimization problem, since the decision variables are functions, rather than real numbers. All solution techniques perform transcription, a process by which the trajectory optimization problem (optimizing over functions) is converted into a constrained parameter optimization problem (optimizing over real numbers). Generally, this constrained parameter optimization problem is a non-linear program, although in special cases it can be reduced to a quadratic program or linear program.

4.2.2.1 Single shooting

Single shooting is the simplest type of trajectory optimization technique. The basic idea is similar to how you would aim a cannon: pick a set of parameters for the trajectory, simulate the entire thing, and then check to see if you hit the target. The entire trajectory is represented as a single segment, with a single constraint, known as a defect constraint, requiring that the final state of the simulation match the desired final state of the system. Single shooting is effective for problems that are either simple or have an extremely good initialization. Both the indirect and direct formulation tend to have difficulties otherwise. [62,66,67].

4.2.2.2 Multiple shooting

Multiple shooting is a simple extension to single shooting that renders it far more effective. Rather than representing the entire trajectory as a single simulation (segment), the algorithm breaks the trajectory into many shorter segments, and a defect constraint is added between each. The result is large sparse non-linear program, which tends to be easier to solve than the small dense programs produced by single shooting. [66,67].

4.2.2.3 Direct collocation

Direct collocation methods work by approximating the state and control trajectories using polynomial splines. These methods are sometimes referred to as direct transcription. Trapezoidal collocation is a commonly used low-order direct collocation method. The dynamics, path objective, and control are all represented using linear splines, and the dynamics are satisfied using trapezoidal quadrature. Hermite-Simpson Collocation is a common medium-order direct collocation method. The state is represented by a cubic-Hermite spline, and the dynamics are satisfied using Simpson quadrature. [62,67].

4.2.2.4 Orthogonal collocation

Orthogonal collocation is technically a subset of direct collocation, but the implementation details are so different that it can reasonably be considered its own set of methods. Orthogonal collocation differs from direct collocation in that it typically uses high-order splines, and each segment of the trajectory might be represented by a spline of a different order. The name comes from the use of orthogonal polynomials in the state and control splines. [67,68].

4.2.2.5 Pseudospectral collocation

Pseudospectral collocation, also known as global collocation, is a subset of orthogonal collocation in which the entire trajectory is represented by a single high-order orthogonal polynomial. As a side note: some authors use orthogonal collocation and pseudospectral collocation interchangeably. When used to solve a trajectory optimization problem whose solution is smooth, a pseudospectral method will achieve spectral (exponential) convergence. [69].

4.2.2.6 Differential dynamic programming

Differential dynamic programming, is a bit different than the other techniques described here. In particular, it does not cleanly separate the transcription and the optimization. Instead, it does a sequence of iterative forward and backward passes along the trajectory. Each forward pass satisfies the system dynamics, and each backward pass satisfies the optimality conditions for control. Eventually, this iteration converges to a trajectory that is both feasible and optimal.[70]

4.2.3 Comparison of techniques

There are many techniques to choose from when solving a trajectory optimization problem. There is no best method, but some methods might do a better job on specific problems. This section provides a rough understanding of the trade-offs between methods.

4.2.3.1 Indirect vs. direct methods

When solving a trajectory optimization problem with an indirect method, you must explicitly construct the adjoint equations and their gradients. This is often difficult to do, but it gives an excellent accuracy metric for the solution. Direct methods are much easier to set up and solve, but do not have a built-in accuracy metric.[62] As a result, direct methods are more widely used, especially in non-critical applications. Indirect methods still have a place in specialized applications, particularly aerospace, where accuracy is critical.

One place where indirect methods have particular difficulty is on problems with path inequality constraints. These problems tend to have solutions for which the constraint is partially active. When constructing the adjoint equations for an indirect method, the user must explicitly write down when the constraint is active in the solution, which is difficult to know a priori. One solution is to use a direct method to compute an initial guess, which is then used to construct a multi-phase problem where the constraint is prescribed. The resulting problem can be solved accurately using an indirect method [62].

4.2.3.2 Shooting vs. collocation

Single shooting methods are best used for problems where the control is very simple (or there is an extremely good initial guess). For example, a satellite mission planning problem where the only control is the magnitude and direction of an initial impulse from the engines [64].

Multiple shooting tends to be good for problems with relatively simple control, but complicated dynamics. Although path constraints can be used, they make the resulting nonlinear program relatively difficult to solve.

Direct collocation methods are good for problems where the accuracy of the control and the state are similar. These methods tend to be less accurate than others (due to their low-order), but are particularly robust for problems with difficult path constraints.

Orthogonal collocation methods are best for obtaining high-accuracy solutions to problems where the accuracy of the control trajectory is important. Some implementations have trouble with path constraints. These methods are particularly good when the solution is smooth.

4.2.3.3 Mesh refinement: h vs. p

It is common to solve a trajectory optimization problem iteratively, each time using a discretization with more points. A h-method for mesh refinement works by increasing the number of trajectory segments along the trajectory, while a p-method increases the order of the transcription method within each segment.

Direct collocation methods tend to exclusively use h-method type refinement, since each method is a fixed order. Shooting methods and orthogonal collocation methods can both use h-method and p-method mesh refinement, and some use a combination, known as hp-adaptive meshing. It is best to use h-method when the solution is non-smooth, while a p-method is best for smooth solutions [69].

4.2.4 Graph theory

In mathematics graph theory is the study of graphs, which are mathematical structures used to model pairwise relations between objects. A graph in this context is made up of vertices, nodes, or points which are connected by edges, arcs, or lines. A graph may be undirected, meaning that there is no distinction between the two vertices associated with each edge, or its edges may be directed from one vertex to another; see Graph (discrete mathematics) for more detailed definitions and for other variations in the types of graph that are commonly considered. Graphs are one of the prime objects of study in discrete mathematics.

4.2.5 Ant Colony

Ant behavior was the inspiration for the metaheuristic optimization technique

In computer science and operations research, the ant colony optimization algorithm (ACO) is a probabilistic technique for solving computational problems which can be reduced to finding good paths through graphs.

This algorithm is a member of the ant colony algorithms family, in swarm intelligence methods, and it constitutes some metaheuristic optimizations. Initially proposed by Marco Dorigo in 1992 in his PhD thesis, [62,63] the first algorithm was aiming to search for an optimal path in a graph, based on the behavior of ants seeking a path between their colony and a source of food. The original idea has since diversified to solve a wider class of numerical problems, and as a result, several problems have emerged, drawing on various aspects of the behavior of ants. From a broader perspective, ACO performs a model-based search [64] and share some similarities with Estimation of Distribution Algorithms.

CHAPTER 5 OUR APPROACH: DJIKSTRA GRID FOR AIRCRAFT TRAJECTORY OPTIMIZATION AND MODELS USED

The approach we use to solve the trajectory optimization problem is graph based and we use several models described in the following paragraph to model aircraft behavior in term of consumption and emissions (models of the aircraft, fuel consumption and emissions, weather and atmosphere).

5.1 Models description

To calculate aircraft emissions (CO2 and NOx) we used EUROCONTROL aircraft BADA model [21], ICAO [27,28] data and NASA Method2Boeing [20]. The aircraft model we have considered is based on BADA (Base of Aircraft Data) developed by Eurocontrol. BADA is a collection of ASCII files that specifies operation performance parameters, airline procedure parameters and performance summary tables for 399 aircraft types.

The most important equations used by the BADA operations performance model is the Total-Energy Model that allows one to compute thrust acting parallel to the **aircraft velocity** vector as a function of true airspeed and rate of climb or descent, in addition to other parameters. From thrust computation, always using BADA models, we can evaluate the fuel flow of the aircraft. For the jet and turboprop engines, the fuel flow is a function of true airspeed and thrust, in addition to other parameters.

5.1.1 Emissions model

Emissions from aircraft originate from fuel burned in aircraft engines. Greenhouse gas emissions are the combustion products and by-products. CO2 and NOX are most important, but also methane, nitrous oxide and other by-product gases are emitted. The fuel use and emissions will be dependent on the fuel type, aircraft type, engine type, engine load and flying altitude.

It is common usage to specify the amount of produced emissions of aircraft engines in the form of so-called emission indices (EI). The EI is the mass of a substance in grams per kilogram of fuel burned [26].

The emission model considered is the Boeing method 2 algorithms [20] for the correction of the ICAO [27,28] engine emission indices in order to take into account weather parameters, such as temperature, pressure and relative humidity at various altitudes.

The Boeing method 2 (BM2) algorithms are used in AEM3[23] for the adjustment of the ICAO NOx, CO and HC engine emission indices to allow for changes in temperature, pressure and relative humidity at altitude.

5.1.1.1 The Boeing 2 Method

The Advanced Emission Model 3 (AEM3) uses a modified version of the Boeing Method 2 (BM2) to estimate emission calculations (NOx, CO and HC).

The International Civil Aviation Organization (ICAO) has established standards and recommended practices (Annex 16 to the ICAO Conference, "Environmental Protection") for the testing of aircraft emissions on turbojet and turbofan engines. The world's jet engine manufacturers have been required to report to ICAO the results of required testing procedures, which pertain to aircraft emissions. ICAO regulations require reporting of emissions testing data on the following gaseous emissions: NOx, HC, CO and smoke. In addition to this, ICAO requires that information be reported on the rate of fuel flow at various phases of flight. Hence, ICAO maintains a database of this where information is available to find out this information for each of the phases of flight as ICAO defines them such Operating Mode Throttle Setting (percent of maximum rated output):

• Take off 100%

- Climb out 85%
- Approach 30%
- Taxi/ground idle 7%

The Boeing Aircraft Company conducted an extensive study for NASA on emission inventories for scheduled civil aircraft worldwide. The Boeing 2 Method is an empirical procedure developed for this study which computes in-flight aircraft emissions using, as a base, the measured fuel flow and the engine ICAO data sheets. Whereas the first Boeing method took into account ambient pressure, temperature and humidity, the second method was more complicated (and accurate). This new method allowed for ambient pressure, temperature and humidity as well as Mach number.

The used methodology to calculate the emissions is reported in [23].

5.1.2 Effects of meteorological changes

With the aim to show the effects of environment, Fig.11 describes how the pressure affects the Emission Index of NOX (EINOX) when the temperature is fixed. The figure shows that for high levels of pressure (during the takeoff or landing phases at ground level) EINOX is quite constant and it is not affected by temperature. On the contrary, for low level of pressure (during cruise level) low differences of temperature cause high difference of EINOX; in particular, they are inversely proportional across the range of 20- 50 kPa (troposphere).



Fig.11 Effect of pressure on emission index of NOx

5.1.3 Noise Model

There are various decibel scales used to define and measure sound in terms that can be related to human perception. An important property of sound is its frequency spectrum – the way that its acoustic energy is distributed across the audible frequency range (from 20 Hz to 20 kHz approximately). Two particular scales are important for aircraft noise - A-weighted sound level and Tone-corrected Perceived Noise Level [31]. The A-weighting is a simple filter applied to sound measurements which applies more or less emphasis to different frequencies to mirror the frequency sensitivity of the human ear at moderate sound energy levels [72]. A-weighted sound level is an almost universally used scale of environmental noise level: it is used for most aircraft noise monitoring applications as well as for the description of road, rail and industrial noise. A-weighted levels are usually denoted as LA. The noise impact assessments that generate the need for noise exposure contours generally rely on A-weighted metrics and these are therefore of primary interest in this guidance; although there are exceptions, Perceived Noise Level applications are confined mostly to aircraft design and certification.

Noise metrics may be thought of as measures of noise 'dose'. There are two main types, describing (1) single noise events (Single Event Noise Metrics) and (2) total noise experienced over longer time periods (Cumulative Noise Metrics).

Noise levels are usually defined at fixed observer locations or mapped as contours (i.e. isolines) depicting the area where the specified levels are exceeded. They are used – especially cumulative metrics - in all domains of transportation noise, in our case air-traffic. These are used to describe the acoustic event caused by a single aircraft movement. Two types are in common usage, both can be determined by measurements as well as by calculations using suitable models (that are the principle subject of this guidance). They are (1) Lmax, based on (1) the maximum sound intensity during the event and (2) LE, based on the total sound energy in the event. The total sound energy can be expressed as the product of the maximum sound intensity and an 'effective duration' of the event.

An aircraft noise event can be described by its observed level-time-history L(t). These are the maximum (frequencyweighted) sound level Lmax and a duration t. Common definitions of the duration are the effective duration, te, i.e. the duration of a noise event with the constant level Lmax that contains the same sound energy as the noise event described by the level-time-history L(t).

Three corresponding single event metrics of particular importance in aircraft noise [73,

74, 75] are (1) Maximum A-weighted Sound level (abbreviation LAmax), (2) Sound Exposure Level (acronym SEL, abbreviation LAE) and (3) Effective Perceived Noise Level (acronym EPNL, abbreviation LEPN). LAmax is still the favored metric for day to day noise monitoring at airports. EPNL is the metric for aircraft noise certification limits laid down by ICAO Annex 16 [75], which all new civil aircraft have to meet. Certification gives noise levels at specific points rather than information on the total noise in the general vicinity of the flight path. An indication of the latter is provided by contours of constant single event noise level - so-called "noise footprints". Noise footprints are useful performance indicators for noise abatement flight procedures since they reflect the impact of noise on the ground of the whole flight path (flight altitude, engine power setting and aircraft speed at all points) rather than only from a part of it. As the decibel scale is logarithmic, long term aircraft noise exposure indices can be logically and conveniently expressed in the form L+ K lg N, where L is the average event level (in decibels of some kind), N is the number of events during the time period of interest, and K is a constant which quantifies the relative importance of noise level and number.

5.1.4 Weather data

In order to compute emissions, the vertical distribution of the following meteorological data is needed: density of air, pressure, temperature, relative humidity, wind speed and direction, and clouds position. These data, except density of the air, are available through numerical weather models that several weather organizations in the world develop for analysis of current situations and forecasts. In our test, only density of the air is computed using the International Standard Atmosphere (ISA) formula.

In the U.S.A., these data are public domain and several different models are available over the Internet, with archives containing all of the data day by day. Among these we chose to use the Rapid Refresh (RAP). The RAP is a NOAA/NCEP operational weather prediction system running every hour that replaced the Rapid Update Cycle (RUC) on 1 May 2012. The RAP is an atmospheric prediction system that consists primarily of a numerical forecast model and an analysis system to initialize the model. Models run hourly, with analysis and hourly forecasts out to 18 hours. RAP files are stored in the GRIB2 file format. GRIB (GRIdded Binary) is a mathematically concise data format commonly used in meteorology to store historical and forecast weather data. The minimum grid spatial resolution is 13 km. In particular, we use a pgrb GRIB2 file that uses 37 vertical levels (isobaric levels) with a grid having a horizontal spatial resolution of 20 km with a dimension of 225x301 grid cells. In order to define clouds, we use the radar reflectivity value.

RAP data can be downloaded from an archive containing datasets for each day/hour of the latest month. Each GRIB file contains the analysis of weather data as it was at that day/hour and the 18 forecasts for the following 18 hours.

This allowed us to evaluate the accuracy of the forecasts by comparing, for example, the weather forecast of 5 p.m. as produced at 3 p.m., with the "real" weather as it was seen in the analysis made at 5 p.m. (2-hour forecast).

5.1.5 Aircraft model

There are several models that can be used to describe an aircraft movement, in accordance to ref. [16,19,21,26] we consider the aircraft, in a 3 Dimension (3D) space with the position described by latitude, longitude and altitude.

Moreover, to obtain a path that minimizes the pollutant emissions, more parameters have to be added to the aircraft description.

The aircraft is modeled as an automaton $A = (X, E, \delta, X_0, X_m, f)$, where:

- X is the finite set of states,
- E is a finite set of events,
- δ is the transition function, described by a state transition directed graph (digraph) G=(X, A) where X={X_i |i = 1,...,N} is the set of nodes, representing all the states of the aircraft in the considered time slice and A={a_ij} is the set of directed arcs, representing the possible transitions of the aircraft.
- X_o is the initial state,
- X_m is the set of final states,
- f is the output function $f: X \times E \to \mathbb{R}^n$ that associates to each state and each event a vector of n components.

The automaton state $X_i = [x_i^1, x_i^2, ..., x_i^K]^T \in X$ is a vector of K components describing the aircraft position and dynamics.

Here, we consider the following K=5 components of the automaton state X_i : x_i^1 (latitude), x_i^2 (longitude), x_i^3 (true altitude), x_i^4 (true airspeed, i.e., TAS), x_i^5 (heading).

The first three variables are required to determine the current position of the aircraft in the space (latitude, longitude and altitude) and the other two components describe the aircraft dynamics aspects (true airspeed and heading).

Such five variables, that in general can assume continuous values, are discretized and, in the adaptive grid, they will be modified to find the smallest graph that can provide accurate

solution. This is reasonable in the considered problem since the scope of this work is determining a flight path composed of a discrete set of waypoints.

Moreover, the event set E is composed by the feasible maneuvers that the aircraft can perform starting from a specific state, and it consists of a set of limited variations of the independent variables.

Furthermore, the transition function δ is described by a state transition directed graph (digraph) G=(X, A) where X={X_i | i = 1, ..., N} is the set of nodes, representing all the states of the aircraft in the considered time slice and A={ a_{ij} } is the set of directed arcs, representing the possible transitions of the aircraft. For the sake of simplicity, the same symbols indicate here digraph nodes and aircraft states. In particular, there exists a directed arc a_{ij} from node X_i to node X_j if there exists a maneuver that allows the aircraft to move from state X_i to state X_j . Moreover, we consider two particular nodes: node X_0 that represents the actual aircraft state (position, true airspeed and heading) and node X_m that represents the final node of the aircraft in the current time slice. Hence, X_m represents the final state of the new trajectory and can be the next planned waypoint or the arrival airport, etc. It is possible that this node could be not precisely identified (position, true airspeed and/or heading are unknown). In this case, it is necessary to determine a set of possible arrival nodes. This set can be composed of nodes that identify different positions, true airspeeds and directions.

Since the automaton \mathcal{A} is a Mealy machine, the automaton outputs can be associated with the digraph arcs.

In the graph an arc does exist if the following four quantities lie within suitable bounds:

- the distance between 2 adjacent nodes;
- the bank angle between the 2 adjacent nodes;
- the speed;
- the altitude variation.

The transition between nodes is computed by using the aircraft performance data and the engine emission model as described in [19], that provide maximum thrust and bank behavior The automaton transition graph models all the possible connections among the states that the aircraft can reach on the basis of the feasible maneuvers (events).

5.1.6 Graph construction

To calculate the emissions associated to the selected trajectory, identify better trajectories in terms of emission reduction and the weights to perform multi-object trajectory optimization,

a graph approach, with algorithms coming from the operational research field are used (i.e. Djikstra, genetic algorithm and Pareto front).

5.1.6.1 Graph construction (base of data of feasible trajectories)

Using the described models and equations, a graph of all feasible trajectories, for the selected aircraft, in a certain volume of space, in which are available the previous listed atmospheric information, is constructed. Such a graph is used to calculated the emissions associated to all the trajectories and to select the better one in terms of emission and noise reduction.

Using aircraft and atmospheric parameters, it is possible to decide whether there is an arc in the graph G. The arch exists if the following four quantities lie within suitable bounds: the distance between 2 adjacent nodes, the bank angle between the 2 adjacent nodes, the speed and the altitude variation. The bounds are determined considering the limitations imposed by the pilot manual [24,25] of the considered aircraft with the selected engines, so the corresponding maneuvers are safe as they are inside the flight envelope of the selected aircraft for the current meteorological conditions.

The Graph is constructed by means of recursive algorithms: starting from a node, all the nodes that are close to it in the components latitude, longitude and altitude, are checked to see if they can be reached and thus the corresponding arc in the Graph exists [19,26]. The reachable states are recursively checked against their neighbors, until all the possible arcs of the Graph are created, obtaining a Graph representative, with its arcs, of a set of feasible trajectories under aircraft constraints.

Hence, the proposed model can consider the avoidance of the No-Flight zones, i.e., regions where flights are not permitted due to bad weather conditions, NOTAM or other conflicts. In order to define No-flight zones, other meteorological data from airborne, ground weather radars, and available forecasts can be used. An arc is removed from the graph if it intersects the forbidden region on the basis of the corresponding spatial coordinates.

In order to construct the graph, we need to define the nodes, the arcs and the weights of the arcs.

The network is directed, there can exist arc (x, y) and arc (y, x) with different weights. Given an arc (x, y), x and y will be referred as tail and head of the arc, respectively.

Input data needed to define the nodes are:

- starting node (S),
- arrival node (A),

- length of the predetermined trajectory between starting and arrival nodes or an evaluation of this length if the predetermined trajectory is unknown,
- desired distance between two consecutive points in the 2D space (ΔX),
- discretization of altitude (ΔZ),
- discretization of true airspeed (Δ S),
- discretization of heading (Δ H),
- mass of the aircraft,
- minimum and maximum values for airspeed,
- minimum and maximum values for altitude,
- meteorological conditions (ISA file).

First, we define the 2D grid of the geographical points, according to ΔX value. Subsequently, each 2D point will be multiplied for the possible values of altitude, true airspeed and heading.

In order to determine the 2D space to be explored, we consider an ellipse with the two fixed points equal to the starting and arrival nodes and the sum of the distances to the two fixed points equal to the length of the predetermined trajectory plus a value of tolerance. In this way, the predetermined trajectory is included in the 2D space. The tolerance value determines the size of the ellipse and also how far can be the new trajectory from the predetermined one.

This 2D space is discretized according to the desired distance between two consecutive points (ΔX). We then obtain a grid used to identify a 2D point.

The number of columns and the number of rows are odd, by construction. Therefore, there is a central column and a central row and the grid can be divided into two parts.

Then, each point in the 2D grid is multiplied for the values of possible altitude, airspeed and heading.

In this way, we have created all the nodes of the graph. We now describe how to compute the arcs of the graph.

The procedure to compute the arcs can be divided into two parts:

- 1. the computation of the arcs starting from nodes of the starting node side,
- 2. the computation of the arcs ending in nodes of the arrival node side.

First, we define the neighborhood of a node: a neighborhood of a node is the set of all nodes "close" to that node. We said that a node is close to another one if in the 2D grid they differ for one row or for one column.

The first procedure (the computation of the arcs starting from nodes of the starting node side) starts exploring the neighborhood of the starting node. For each node of its neighborhood, let say y, we verify if there can be an arc between the starting node and y (we will explain later how to verify if an arc exists). If the arc exists it is added to the network and, if node y satisfies some constraints, it is saved as node to be explored. After the exploration of all nodes of the neighborhood of the starting node, we choose a node to be explored and we repeat the same procedure (exploration of all nodes of its neighborhood). The procedure ends when there are no nodes to be explored.

The second procedure (the computation of the arcs ending in nodes of the arrival node side) is similar to the first procedure. We still explore a neighborhood, but a node has to satisfy other constraints to be saved as node to be explored. We start exploring the neighborhood of the arrival node, verifying if from a node of its neighborhood the arrival node can be reached. If it is the case, the arc is added to the network and the node, if it satisfies some constraints, is saved as node to be explored.

In general, a node can be inserted between the node to be explored if it has not been explored and if it is in the starting node side (first procedure) or in the arrival node side (second procedure).

The computation of the weights of the arcs is connected with the check if an arc exists.

For each couple of nodes, we compute the needed thrust to fly between the two nodes. Subsequently, given the thrust and other meteorological parameters it is possible to compute emissions.

We now describe the procedure to compute the needed thrust between two nodes.

- 3. compute the distance between the two nodes given the coordinates and the altitude.
- 4. compute the course angle between the two points (direction to be followed)
- 5. compute the average of true airspeed
- 6. compute ground speed and correction angle (due to wind) using course angle, average true airspeed and wind data (speed and direction)
- 7. compute travel time given ground speed and distance
- 8. compute correction of heading given the current heading and the correction angle
- 9. compute rate of turn given heading variation and travel time of the arc
- 10. compute bank angle given rate of turn and average true airspeed
- 11. compute thrust given distance, true airspeed in the two nodes, altitude in the two nodes, bank angle, travel time, flight phase, mass of the aircraft and meteorological parameters.

Each component of the state vector are parametrized taking into account min value, max value, step resolution named respectively, for i: 1..5, XiMin; XiMax; DXi. To determine the better graph in terms of minimum dimensions for the required accuracy all the previous parameters will be automatically varied till some stop criteria will be reached.

The chosen stop criteria are:

- DXi reached selected thresholds depending on the phase of flight;

- The fuel consumption doesn't increase anymore for 3 consecutive steps
- The mean and mode of the maximum and minimum altitude doesn't increase for 3 consecutive steps.

In the following picture is represented a typical aircraft trajectory with the variables limits (XiMin; XiMax).



Fig.12 Aircraft trajectory with A320 typical performance parameters (maximum and Minimum speed, altitude, climb time and distance)

5.1.6.2 Dijkstra based trajectory optimizer

Dijkstra's algorithm finds the shortest path from the source node v1 to all other nodes in a network with nonnegative arc weights [29]. Dijkstra's algorithm maintains a distance label d(i) with each node i, which is an upper bound on the shortest path cost to node i.

At any intermediate step, the algorithm divides the nodes into two groups: those which it designates as permanently labeled (or permanent) and those it designates as temporarily labeled (or temporary). The distance label to any permanent node represents the shortest distance from the source to that node. For any temporary node, the distance label is an upper bound on the shortest path distance to that node.

The basic idea of the algorithm is to fan out from node v1 and permanently label nodes in the order of their distances from node v1. Initially, we give node v1 a permanent label of zero, and each other node j a temporary label equal to ∞ . At each iteration, the label of a node i is its shortest distance from the source node along a path whose internal nodes (i.e., nodes other than v1 or the node i itself) are all permanently labeled.

The algorithm selects a node i with the minimum temporary label, makes it permanent, and reaches out from that node, that is, scans arcs in A(i) (arcs outgoing from node i) to update the distance labels of adjacent nodes.

The algorithm terminates when it has designated all nodes as permanent. The correctness of the algorithm relies on the key observation that we can always designate the node with minimum temporary label as permanent.

The pseudo-code of Dijkstra's algorithm is report in the following:

```
algorithm Dijkstra

begin

S := \emptyset; \overline{S} := N;

d(i) := \infty for each node i \in N;

d(s) := 0 and pred(s) := 0;

while |S| < n do

begin

let i \in \overline{S} be a node for which d(i) = \min\{d(j) : j \in \overline{S}\};

S := S \cup \{i\};

\overline{S} := \overline{S} \cup \{i\};

for each (i, j) \in A(i) do

if d(j) > d(i) + c_{ij} then d(j) := d(i) + c_{ij} and pred(j) := i;

end;

end;
```

5.1.6.3 Genetic based trajectory optimizer

The genetic optimization algorithm is a search heuristic algorithm simulating the process of natural evolution. This algorithm is routinely used to generate useful solutions to searching and optimization problems. Genetic algorithms belong to the larger class of Evolutionary Algorithms (EA) generating solutions to optimization problems using several methods inspired by natural evolution, such as inheritance, mutation, selection, and crossover.

In a genetic optimization algorithm, a population of strings (called chromosomes or the genotype of the genome), which encode candidate solutions (called individuals, creatures, or phenotypes) to an optimization problem, evolves toward better solutions. Traditionally, solutions are represented in binary format as strings of os and 1s, but other encoding methods may be used. The evolution usually starts from a population of randomly generated individuals and happens in generations. In each generation, the fitness of every individual in the population is evaluated, multiple individuals are stochastically selected from the current

population (based on their fitness), and modified (recombined and possibly randomly mutated) to form a new population. The new population is then used in the next iteration of the algorithm. Usually, the algorithm stops when either a satisfactory fitness level has been reached for the population or a maximum number of generations has been reached. In this case of ending due to the reaching of the maximum number of generations, a satisfactory solution may or may not be achieved.

As detailed below, a simple generational genetic algorithm pseudo-code is:

1. Choose the initial population of individuals

2. Evaluate the fitness of each individual in that population

3. Repeat on this generation until termination: (time limit, sufficient fitness achieved, etc.)

4. Select the best-fit individuals for reproduction

5. Breed new individuals through crossover and mutation operations to give birth to

6. offspring

7. Evaluate the individual fitness of new individuals

8. Replace least-fit population with new individuals

Hence typical genetic algorithm requires:

- a genetic representation of the solution domain

- a fitness function to evaluate the solution domain.

5.1.6.4 Multi-objective trajectory optimization

To perform multi-object trajectory optimization, the different optimization objective are weighted by a value between 0 and 1 and the sum of the weights is 1. After the weights are applied the trajectory optimization algorithm is performed.

5.1.6.5 Generation of Non-dominated solutions: Pareto

The optimization of fuel consumption (proportional to CO₂ emission), NO_x and Noise in many cases and phase of flight are concurrent [30], so it is not so easy to find a way to optimize together all the 3 emissions.

In general, for a nontrivial multi-objective optimization problem, there does not exist a single solution that simultaneously optimizes each objective. In that case, the objective functions are said to be conflicting, and there exists a (possibly infinite number of) Pareto optimal solutions. A solution is called non-dominated, Pareto optimal, Pareto efficient or non-inferior, if none of the objective functions can be improved in value without impairment in some of the other objective values. Without additional preference information, all Pareto optimal solutions can be considered mathematically equally good (as vectors cannot be

ordered completely). The set of Pareto optimal solutions is often called the Pareto front. The methodology proposed in this thesis aims at combining the set of emissions computed during a flight phase (the results in climb phase are reported below), considering the aircraft moving from an initial waypoint toward a final waypoint. The emissions, that typically have different units of measurement and different ranges, have been normalized considering the typical range of emissions in that flight phase as described in the ICAO databank for CO2 [27,28], the Boeing model for NOX [23] and the DOC29 [34] for Noise. The aircraft model used in the simulation is derived by BADA database [21] for A320. The optimized trajectory is then used to compute the emissions in climb phase given that set of weights. Changing the set of weights at the input and computing the corresponding optimized trajectories and related emissions, it is possible to determined what set of weights produces non-dominated Pareto solution. Repeating this computation on different flights and different weather condition, it is possible to study what is the best set of weights for that type of aircraft. The main contribution of this thesis is to investigate the optimal values for the emissions weights in a specific climb phase. In general more than one solution was obtained and the decision maker, typically the flight company, can choose which pollutant is more important to be reduced in that flight area and determine the cost index.

The Pareto optimal solution method is tested on the climb phase of the trajectory of an A320, DAL1451 (from Flightaware), in USA and using the real atmospheric condition contained in a GRIB file downloaded from NOAA database to calculate the emissions. The multi-objective function was computed using a linear combination of the three pollutants: CO2, NOx and Noise. The weights for each pollutant in the optimization algorithm are chosen between 0.1 and 0.8 and the sum of the three weights is one.

CHAPTER 6 RESULTS OF TRAJECTORY OPTIMIZER APPLIED TO REAL SCENARIOS WITH UNFORESEEN WEATHER EVENTS

In the present section are reported different kind of results related to the proposed trajectory optimizer. In the first part the weather prediction reliability is considered. It is demonstrated that the weather predictions (especially the weather reflectivity and the wind) are not enough reliable for a preplanned optimized trajectory, but it is necessary to provide an on-board real time trajectory optimization. Then two use cases, in real conditions, with an A320 in climb and in cruise phases, are analyzed, the optimized trajectories, with different optimization target, are provided and the results are compared with the real flight, showing the possibility of a big potential emission reduction improvements. Then the multi-objective trajectory optimizer is considered and the different emission results associated to the optimized trajectories obtained with different emission weights, are provided, and compared. Set of emission weights that provided the same results in terms of emissions, and that provided the minimum emissions of the selected pullant, are identified. Then the obtained using different weather models are compared and the different results are underlined. Finally, it is proposed
a flight simulator, based on X-Plane, as tool to validate the data. As it is shown later, the results obtained are quite promising.

For the calculation, only aircraft climb and cruise phases are taken into account, because they are the only one in which it is possible to obtain a relevant decrease of fuel consumption and emissions, while in descent phase generally the pilot perform a continuous descent approach with the engine in idle mode, so there are no big margins of possible improvements.

6.1 Weather prediction reliability

As mentioned before, trajectory optimization is highly sensitive to weather conditions; pressure, relative humidity, wind intensity and direction have various influences on thrust conditions and emissions [19]. In this section, real atmospheric conditions and real flight trajectory are used to evaluate the performance of our algorithm for trajectory optimization and to calculate and compare emissions associated to different trajectories (real one and optimized ones). In particular, some test cases, related to different phase of flight and based on real data downloaded from USA internet archives, are described and the results, of the application of optimizer to these test cases, are reported.

The reference weather models used to define the following test cases are the ones produced by the National Oceanic and Atmospheric Administration (NOAA), a U.S.A. federal agency focused on the condition of the oceans and the atmosphere. They distribute several weather model datasets [11] upon different domains and most data, due to U.S. federal law, are available as public domain.

From the NOAA archives, the RAP (Rapid Refresh) hourly-updated model weather prediction was used. RAP model and its data are most likely the state of the art regarding reliable weather information for aircraft use available as public domain.

In the following test cases, we used RAP weather datasets with 20 Km spatial resolution and 50 altitude levels, downloaded from the NOAA archive that contains datasets for each day/hour of the latest month. Each GRIB (Gridded Binary) file contains the analysis of weather data as it was at that day/hour and the 18 forecasts for the following 18 hours. That allows to evaluate the accuracy of the forecasts, by comparing the predicted weather forecast, referred to different hours, with the "real" weather. The days evaluated are 17/18/19/20 June 2012, the results are reported below and they show that for some parameters (T, P, etc.) the predictions are reliable, for other parameters (reflectivity, wind) more than 1h predictions are not reliable and it shouldn't be used for trajectory optimization. These unpredictable parameters produce the "unforeseen" weather events the pilot should cope with. Unforeseen

reflectivity and wind changes are some of the events used to start Q-AI for trajectory optimization calculations.

6.1.1 evaluation of weather prediction Accuracy

Weather reflectivity and wind (speed and direction) are 2 of the events that starts Q-AI calculation and are used for trajectory optimization. These data can be obtained from a webserver or on-board from weather radar (reflectivity and radial wind intensity).

The reflectivity provided by the radar is usually described by colour or level. The colours in a radar image normally range from blue or green for weak returns, to red or magenta for very strong returns. The numbers in a verbal report increase with the severity of the returns. For example, the U.S. National Doppler Radar sites use the following scale for different levels of reflectivity:

- magenta: 65 dBZ (extremely heavy precipitation, possible hail)
- red: 52 dBZ
- yellow: 36 dBZ
- green: 20 dBZ (light precipitation)

Strong returns (red or magenta) may indicate not only heavy rain but also thunderstorms, hail, strong winds, or tornadoes, but they need to be interpreted carefully (annex A).

When describing weather radar returns, pilots, dispatchers, and air traffic controllers will typically refer to three return levels:

- level 1 corresponds to a green radar return, indicating usually light precipitation and little to no turbulence, leading to a possibility of reduced visibility.
- level 2 corresponds to a yellow radar return, indicating moderate precipitation, leading to the possibility of very low visibility, moderate turbulence and an uncomfortable ride for aircraft passengers.
- level 3 corresponds to a red radar return, indicating heavy precipitation, leading to the possibility of thunderstorms and severe turbulence and serious structural damage to the aircraft.

An example of the parameter "MaximumComposite_Radar_Reflectivity", taken from the GRIB file for 18/6/2012 at 3 a.m (current weather field), is shown in the figure 1 below. In the figure the reflectivity values are in dBZ and the colors follow the rainbow colormap values at the right of the figure. The considered GRIB file was downloaded from NOAA site, in particular from CONUS (Continental United States) domain for RAP model with 225x301 grid points.



Fig.13 Weather reflectivity on USA the 18/6/2012 at 3 a.m

6.1.1.1 Reflectivity forecast accuracy

In order to evaluate accuracy of forecasts regarding evaluation of the presence of bad weather (level 1, reflectivity > 20 dBZ), or potentially severe weather condition (level 2 or more, then reflectivity level > 36 dBZ), a threshold filter was applied to reflectivity data (current data and forecasted ones related to the same hour) to select regions with reflectivity above 20 dBZ (fig 3) and above 36 dBz.

In figures below an example of a rainbow color map representation analysis, of current weather at 10 a.m. 19/06/2012, and the 1-hour forecast made at 9 a.m. is reported (Fig. 14).



Fig.14 Real and forecasted reflectivity on USA the 18/6/2012 at 3 a.m

In the following figure are represented the same data with the reflectivity threshold of **20** dBz applied.



Fig.15 Real and forecasted reflectivity above 20 dBz on USA the 18/6/2012 at 3 a.m

Comparing the two images it is possible to identify a large zone with high reflectivity that in forecast was "clear". Conventionally this situation is called a "miss" of FN: "False Negative". In other examples, instead, it was possible to idenfify zones with high reflectivity forecast that in real weather (analysis) resulted clear ("false alarm", conventionally called FP: "False Positive").

In the image below the comparison between the 2 previous images is reported (in red the "perfect forecast" or TP: True Positive, in cyan the difference).



Fig.16 Comparison Real (analysis, cyan) and forecasted (1h before) reflectivity

A widely-used index for measuring accuracy in a region recognition in images is the Jaccard-Tanimoto Index. Given the exact shape on grid of the region (in this case, the current weather analysis) and its approximation (in this case the forecast), the Tanimoto Index TI is defined as TI = TP/(FP+FN+TP) or, in other words, the number of "pixels" of intersection on the number of pixels of the union of the two images. A TI of 85-90% or above is usually considered, in image segmentation, a very accurate result.

We compared each one of the weather analysis (current weather) in the 4 days considered (96 hours total) with the forecasts for that time from 1 to 6 hours before; then we computed Tanimoto index for each and the total clouds coverage. These calculations were made for the data with threshold at 20 dBZ (level 1 or more clouds) and for the data with threshold at 36 dBZ (level 2 or more clouds).

In table below are reported the average results:

	Jaccard-Tanimoto Index – 20 dBZ threshold								
	1.Hour	2.Hour	3.Hour	4.Hour	.5Hour	6.Hour			
Clouds	Forecast	Forecast	Forecast	Forecast	Forecast	Forecast			
0,094122	0,910662	0,596208	0,469113	0,391596	0,33863	0,301704			
	Jaccard-Tanimoto Index – 36 dBZ threshold								
Clouds	1.Hour	2.Hour	3.Hour	4.Hour	5.Hour	6.Hour			
Clouds	Jaccard-Tanim	oto Index – 36 dl 2.Hour	BZ threshold 3.Hour	4.Hour	5.Hour	6.Hour			

	Forecast	Forecast	Forecast	Forecast	Forecast	Forecast
0,004701	0,812975	0,433031	0,260201	0,159075	0,099386	0,067976

Table 2 Clouds reflectivity prediction reliability

It can be seen that the weather forecast accuracy at 1 hour is quite good, but it becomes much worse very quickly. Only forecasts not older than 1 hour should be used in order to plan trajectories with a reliable knowledge about the "no flight zones" due to severe weather conditions.

6.1.1.2 Wind forecast accuracy

The same calculations were done also for wind direction and speed in the same days (applying a threshold to wind speed and direction to evaluate the changes). The data were selected from the same GRIB files used before. The results present a behavior, in data prediction accuracy over time, similar to the reflectivity.

6.2 Trajectory optimization Test cases

In this paragraph are considered 2 test cases (in climb and cruise phases) that will be considered also in Chapter 7 for the real-time graph generation proposed method. The 2 test cases consist in real flights of civil aircraft in real weather conditions. The emissions related to the optimized trajectories are compared with the emissions related to the real trajectories showing that there is a big margin of possible improvement.

6.2.1 Test Case 1

In this first test case is considered the real trajectory (downloaded from flightaware archive) of an A320 (DAL1888) in cruise phase in real weather conditions (downloaded from NOAA archive). In the following paragraphs, the emissions associated to the real aircraft trajectory and the trajectories optimized in accordance to different criteria are provided and compared. The considered trajectory is originated from the International Airport of Las Vegas (KLAS) (36.080°, -115.152°) on November 11th 2012 at about 4 p.m. (UTC): DAL1888. This flight is directed to the International Airport of Memphis. It is considered a part of the cruise phase of the trajectories. We suppose that the mass of the aircraft is 64000 kg.

6.2.1.1 Meteorological data

Meteorological data are RAP data of November 11th, 2012 at 6 p.m. (UTC). Wind speed and direction at altitude equal to about 10668 m are depicted in the following figure.



Fig.17 The Wind speed, direction, and intensity (different colors) at 10668 m.

6.2.1.2 Route and aircraft emissions

In the following table are reported the starting and ending points of the climb phase of the three considered trajectories.

Start Lat (°)	Start Lon (°)	Start Alt (m)	End Lat (°)	End Lon (°)	End Alt (m)
35.35	-99.4642	10637	35.4783	-94.3931	10668

Table 3 Initial and final position of DAL1888 trajectory considered

In the following figure, we represent the normal flight (November 9th 2012 at 4:31 p.m. UTC), the flight of the test 3 and clouds (maximum radar reflectivity) of November 11th 2012 at 6 p.m. UTC. The normal flight is the black one and the tested flight is the red one. We represent clouds at 6 p.m. UTC since 6 p.m. UTC is the time in which the flight plan is going close to clouds.



Fig.18 DAL1888 real flights (black one usual, red one particular deviation tested)

In the following figure, we represent the same trajectories but clouds expected at 6 p.m. UTC computed at 1 p.m. UTC (computed about 3 hours before the takeoff). From the figure one can note that the normal trajectory flights close to dangerous clouds.



Fig.19 DAL1888 real flights (black one usual, red one tested)

In order to compute noise emissions three observation points are set: Minneapolis (44.993N, -93.265E), St. Paul (44.9536N, -93.092E) and Rochester (44.031N, -92.467E).

The real trajectory is taken from "FlightAware" website (<u>http://flightaware.com</u>).

6.2.1.3 Test results

In the following table the aircraft emissions are reported. For the Multi-objective function the weight of CO2 and NOx emissions is the same.

The differences in the calculated emissions depend mainly on wind and cloud reflectivity values that are not so reliable for what concern the prediction [19]. On the other side, pressure, temperature, and humidity prediction are more reliable [19].

Using the weighted Graph of the feasible trajectories, are calculated the emissions associated to different trajectories. In table 3 are reported the emissions associated to the real flight (column 2 in table 4) and the ones associated to optimized trajectories, applying Dijkstra mono or multi-object and a genetic algorithm to select an optimized trajectory in accordance to different criteria (table 4, in column 3 Dijkstra Mono-objective CO2, 4 Dijkstra Mono-objective NOx, 5 Dijkstra Multi-objectives, 6 Genetic Multi-objective). The multi-objective trajectory optimization is calculated attributing to NOx and CO2 emissions a weight of 0.5 each.

	FA	Dijkstra's	Dijkstra's algorithm			
		CO2	NOx	МО	МО	
CO2 (kg)	4002	3472	3528	3528	3528	
NOx (kg)	23.98	20.32	19.41	19.41	19.41	
CPU time (s)		3991				
(network constr.)						
CPU time (s)		0.23	0.23	0.23	77.81	
(optimization algorithm)						

Table 4 DAL1888 emissions and emission associated to optimized trajectories



Fig.20 Real trajectory (black) performed by DAL1888 and optimized trajectories (waypoints blue and red)

6.2.2 Test Case 2

In this first test case is considered the real trajectory (downloaded from flightaware archive) of an A320 (DAL1760) in climb phase in real weather conditions (downloaded from NOAA archive). In the following paragraphs, the emissions associated to the real aircraft trajectory and the trajectories optimized in accordance to different criteria are provided and compared. An A320, DAL1760 emissions in climb phase in real weather conditions.

The considered trajectory is originated from Minneapolis/St Paul International Airport (KMSP) (44.88°, -93.22°) on June 18th 2012 at about 03 a.m. (UTC): DAL1760. It is considered the climb phase, until cruise flight level is reached. We consider the aircraft weights equal to 64000 kg.

6.2.2.1 Meteorological data

Meteorological data are RAP data of June 18th, 2012 at 03.00 am (UTC) (available here: http://motherlode.ucar.edu:8080/thredds/catalog/fmrc/NCEP/RAP/CONUS_20km/files/c atalog.html). Wind speed and direction at altitude equal to about 3000 m and 8000 m are depicted in the following figures.



Fig.21 The Wind speed, direction and intensity (different colors) at 3000 m.



Fig.22 The Wind speed, direction and intensity (different colors) at 8000 m.

6.2.2.2 Route and aircraft emissions

In the following table are reported the starting and ending points of the climb phase of the three considered trajectories.

Start Lat (°)	Start Lon (°)	Start Alt (m)	End Lat (°)	End Lon (°)	End Alt (m)
44.8258	-93.2317	945	44.1100	-95.8472	10973

Table 5 Initial and final position of DAL1760 trajectory considered

In order to compute noise emissions three observation points are set: Minneapolis (44.993N, -93.265E), St. Paul (44.9536N, -93.092E) and Rochester (44.031N, -92.467E).

The real trajectories are taken from "FlightAware" website (http://flightaware.com).

In the following figure (Fig.3) the "normal" trajectory (in this case the trajectory of June 17th 2012 at about 03 a.m.) (blue) and the trajectory of June 18th 2012 (black) are depicted, related to real cloud reflectivity the June 18th 2012 at 03 a.m.



Fig.23 Two trajectories performed by DAL1760 in different days and atmospheric conditions are reported.

In the following tables, emissions of the aircraft are reported. In table 6 the estimated emissions of the trajectory in different atmospheric conditions are reported. In particular, are calculated the emissions associated to the same trajectory with the real meteorological conditions and the ones forecasted one, three and six hours before, in order to assess the impact of meteorological conditions on the emissions.

DAL1760	DAL1760 Real		3 h	6 h
	meteo	forecast	forecast	forecast
CO2 (kg)	5220	5172	5181	5198
NOx (kg)	66.54	63.76	63.36	63.02

Table 6 estimated emissions of DAL1760 in different atmospheric conditions

The differences in the calculated emissions depend mainly on wind and cloud reflectivity values that are not so reliable for what concern the prediction [19]. On the other side, pressure, temperature and humidity prediction are more reliable [19].

Then, using the weighted Graph of the feasible trajectories, are calculated the emissions associated to different trajectories. In table 7 are reported the emissions associated to the real flight (column 2 in table 3) and the ones associated to optimized trajectories, applying Dijkstra mono or multi-object and a genetic algorithm to select an optimized trajectory in accordance to different criteria (table 7, in column 3 Dijkstra Mono-objective CO2, 4 Dijkstra Mono-objective NOx, 5 Dijkstra Multi-objectives, 6 Genetic Multi-objective). The multi-objective trajectory optimization is calculated attributing to NOx and CO2 emissions a weight of 0.5 each.

	FA	Dijkstra's	GA		
		CO2	NOx	M01	M01
CO2 (kg)	5220	4699	5907	4758	5453
NOx (kg)	66.54	87.85	51.02	53.81	61.05
CPU time (s)	4622				
(network constr.)					
CPU time (s) (optimization algorithm)		0.15	0.15	0.15	44.4

Table 7 DAL1760 emissions and emission associated to optimized trajectories

6.3 Trajectory optimization with emissions weights

In this first test case is considered the real trajectory (downloaded from flightaware archive) of an A320 (DAL1451) in climb phase in real weather conditions (downloaded from NOAA archive). In the following paragraphs, the emissions associated to the real aircraft trajectory and the trajectories optimized in accordance to different criteria are provided and compared. An A320, DAL1451 emissions in climb phase in real weather conditions.

The considered trajectory is originated from Minneapolis/St Paul International Airport (KMSP) (44.88°, -93.22°) on June 18th 2012 at about 03 a.m. (UTC): DAL1451. It is considered the climb phase, until cruise flight level is reached. The aircraft is A320 and it is supposed that its mass is 64000 kg.

6.3.1 Meteorological data

Meteorological data are RAP data of June 18th, 2012 at 03.00 am (UTC) (available here: http://motherlode.ucar.edu:8080/thredds/catalog/fmrc/NCEP/RAP/CONUS_20km/files/c atalog.html). Wind speed and direction at altitude equal to about 3000 m and 8000 m are depicted in the following figures.



Fig.24 The Wind speed, direction, and intensity (different colors) at 3000 m.



Fig.25 The Wind speed, direction, and intensity (different colors) at 8000 m.

6.3.2 Route and aircraft emissions

In the following table are reported the starting and ending points of the climb phase of the three considered trajectories.

Start Lat (°)	Start Lon (°)	Start Alt (m)	End Lat (°)	End Lon (°)	End Alt (m)
44.82	-93.23	914	43.33	-95.91	10363

Table 8 Initial and final position of DAL1451 trajectory considered

In order to compute noise emissions three observation points are set: Minneapolis (44.993N, -93.265E), St. Paul (44.9536N, -93.092E) and Rochester (44.031N, -92.467E).

The real trajectories are taken from "FlightAware" website (http://flightaware.com).

In the following figure (Fig.3) the "normal" trajectory (in this case the trajectory of June 17th 2012 at about 03 a.m.) (blue) and the trajectory of June 18th 2012 (black) are depicted, related to real cloud reflectivity the June 18th 2012 at 03 a.m.



Fig.26 Two trajectories performed by DAL1451 in different days and atmospheric conditions are reported.

In the following tables, emissions of the aircraft are reported. In table 2 the estimated emissions of the trajectory in different atmospheric conditions are reported. In particular, are calculated the emissions associated to the same trajectory with the real meteorological conditions and the ones forecasted one, three and six hours before, in order to assess the impact of meteorological conditions on the emissions.

DAL1451	AL1451 Real		3 h	6 h
	meteo	forecast	forecast	forecast
CO2 (kg)	5366	5315	5323	5307
NOx (kg)	62.99	59.76	59.98	59.63
Noise	53.33	53.18	53.03	52.93
(dB)				

Table 9 estimated emissions of DAL1451 in different atmospheric conditions

The differences in the calculated emissions depend mainly on wind and cloud reflectivity values that are not so reliable for what concern the prediction [19]. On the other side, pressure, temperature, and humidity prediction are more reliable [19].

Then, using the weighted Graph of the feasible trajectories, are calculated the emissions associated to different trajectories. In table 10 are reported the emissions associated to the real flight (column 2 in table 3) and the ones associated to optimized trajectories, applying Dijkstra mono or multi-object and a genetic algorithm to select an optimized trajectory in accordance to different criteria (table 3, in column 3 Dijkstra Mono-objective CO2, 4 Dijkstra Mono-objective NOx, 5 Dijkstra Multi-objectives, 6 Genetic Multi-objective). The multi-

	FA emit	Dijkstra's a	Dijkstra's algorithm				
		CO2	NOx	Noise	MO	МО	
CO2 (kg)	5366	5204	6370	6897	5255	5266	
NOx (kg)	62.99	88.28	52.24	112.08	53.81	61.05	
Noise (dB)	53.33	61.60	49.45	45.58	51.38	49.02	

objective trajectory optimization is calculated attributing to NOx, CO2 and Noise emissions a weight of 0.4, 0.4, 0.2.

Table 10 DAL1451 emissions and emission associated to optimized trajectories

6.3.3 Comparing multi-objective trajectories using Pareto front

The optimization of more than one objective sets a problem on how to combine the single objectives in order to find a satisfactory solution. In the reported tests the three pollutants (CO2, NOx and Noise) were combined using a linear combination. Varying and combining the different weights it was possible to find a set of solutions "ordered" using the definition of Pareto optimal solutions often called Pareto Front.

This method was tested on the climb phase of the trajectory DAL1451. The multi-objective function was computed using a linear combination of the three pollutants: CO2, NOx and Noise. The weights for each pollutant in the objective function used by Dijkstra's algorithm are between 0.1 and 0.8 and the sum of the three weights must be one. The objective function used by Genetic algorithm takes into account the linear combination of the three pollutants (as explained for Dijkstra's algorithm) and also the number of consecutive turns.

In the following table the 36 solutions found using Dijkstra algorithm are reported. The first three columns report the weights used in the multi-objective function, the successive three columns report the value of the three pollutants computed. In bold are reported the solutions belonging to the Pareto front. In the tables are underlined in green the solutions with minimum CO₂ emission, in pink the solutions with minimum NO_x, in cyan the solutions with minimum Noise; in dark green the solutions with minimum CO₂ for min NOX and Noise [30].

Dijkstra Pareto Front							
CO2	NOx	Noise	CO2	NOx	Noise		
0.1	0.1	0.8	5812.52	54 87	Emission 48.80		
0.1	0.2	0.7	5866.44	53.92	48.81		
0.1	0.3	0.6	5866.44	53.92	48.81		
0.1	0.4	0.5	5978.30	53.33	48.81		
0.1	0.5	0.4	6061.76	52.97	48.82		
0.1	0.6	0.3	6241.41	<mark>52.38</mark>	48.77		
0.1	0.7	0.2	6241.41	<mark>52.38</mark>	48.77		
0.1	0.8	0.1	6241.41	<mark>52.38</mark>	<mark>48.77</mark>		
0.2	0.1	0.7	5506.27	62.52	51.29		
0.2	0.2	0.6	5812.52	<mark>54.87</mark>	48.80		
0.2	0.3	0.5	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.2	0.4	0.4	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.2	0.5	0.3	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.2	0.6	0.2	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.2	0.7	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.3	0.1	0.6	<mark>5437.68</mark>	64.85	54.63		
0.3	0.2	0.5	<mark>5557.44</mark>	60.71	51.29		
0.3	0.3	0.4	5697.09	56.96	51.30		
0.3	0.4	0.3	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.3	0.5	0.2	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.3	0.6	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.4	0.1	0.5	5372.47	68.96	54.68		
0.4	0.2	0.4	<mark>5472.44</mark>	63.30	54.63		
0.4	0.3	0.3	5697.09	56.96	51.30		
0.4	0.4	0.2	5697.09	56.96	51.30		
0.4	0.5	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>		
0.5	0.1	0.4	5296.21	75.87	54.70		
0.5	0.2	0.3	<mark>5437.68</mark>	64.85	54.63		
0.5	0.3	0.2	5557.44	60.71	51.29		
0.5	0.4	0.1	5697.09	56.96	51.30		
0.6	0.1	0.3	5244.65	80.49	57.77		
0.6	0.2	0.2	5437.68	64.85	54.63		
0.6	0.3	0.1	5472.44	63.30	54.63		
0.7	0.1	0.2	5244.65	80.49	57.77		
0.7	0.2	0.1	5397.78	67.14	54.65		
0.8	0.1	0.1	<mark>5244.65</mark>	80.49	57.77		

Table 11 Emissions associated to multi-object Dijkstra optimized trajectories

In the following table the 36 solutions found using Genetic algorithm are reported. The first three columns report the weights used in the multi-objective function, the successive three columns report the value of the three pollutants computed. In bold are reported the solutions belonging to the Pareto front.

	Genetic Pareto Front								
CO2 weight	NOx weight	Noise weight	CO2 emission	NOx emission	Noise Emission				
0.1	0.1	0.8	5855.31	56.89	50.19				
0.1	0.2	0.7	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.1	0.3	0.6	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.1	0.4	0.5	5978.30	<mark>53.33</mark>	48.81				
0.1	0.5	0.4	6119.26	<mark>53.10</mark>	<mark>47.92</mark>				
0.1	0.6	0.3	5999.97	55.36	50.21				
0.1	0.7	0.2	6119.27	<mark>53.17</mark>	<mark>48.84</mark>				
0.1	0.8	0.1	6172.95	<mark>53.26</mark>	<mark>47.95</mark>				
0.2	0.1	0.7	5546.12	61.57	52.14				
0.2	0.2	0.6	5669.47	58.79	52.13				
0.2	0.3	0.5	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.2	0.4	0.4	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.2	0.5	0.3	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.2	0.6	0.2	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.2	0.7	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.3	0.1	0.6	5900.51	62.25	<mark>48.80</mark>				
0.3	0.2	0.5	5625.76	59.75	51.30				
0.3	0.3	0.4	5785.34	56.68	52.11				
0.3	0.4	0.3	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.3	0.5	0.2	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.3	0.6	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.4	0.1	0.5	5384.73	71.16	54.67				
0.4	0.2	0.4	5632.85	59.12	51.28				
0.4	0.3	0.3	<mark>5476.67</mark>	64.35	54.66				
0.4	0.4	0.2	5809.84	55.38	<mark>48.84</mark>				
0.4	0.5	0.1	5866.44	<mark>53.92</mark>	<mark>48.81</mark>				
0.5	0.1	0.4	5296.21	75.87	54.70				
0.5	0.2	0.3	5766.74	58.20	52.09				
0.5	0.3	0.2	5632.85	59.12	51.28				
0.5	0.4	0.1	5783.44	57.01	50.18				
0.6	0.1	0.3	<mark>5244.65</mark>	80.49	57.77				
0.6	0.2	0.2	5560.73	64.46	54.66				
0.6	0.3	0.1	5444.42	66.76	52.18				
0.7	0.1	0.2	<mark>5244.65</mark>	80.49	57.77				
0.7	0.2	0.1	5204.02	88.28	61.61				
0.8	0.1	0.1	5244.65	80.49	57.77				

Table 12 Emissions associated to multi-object Genetic optimized trajectories

It is possible to notice that in the selected case the Minimum Noise emission is connected to the minimum NOx emission (generally both are minimized in case of constant engine regime). On the contrary Fuel consumption (and CO2 that is proportional by a factor of 3.18) are minimized when NOx and Noise increase.

It is possible to identify some cases (underlined in dark green in table 4 and 5) in which there is a limited emission of CO₂ (fuel consumption) in correspondence of low emission of NOx and Noise. Generally, the decision maker (i.e. the flight company) chooses the trajectory emission index and the weights and the criteria to be used to optimize the trajectory.

6.4 Trajectory optimization with different weather model and emissions weights

In the present paragraph, the results obtained applying, the described methods, to an A320, in climb phase in real atmospheric condition, are presented. The considered trajectory is originated from the International Airport of Fort Lauderdale-Hollywood (KFLL) on April 3rd 2013 at about 01 p.m. (UTC): NKS724. It is considered the climb phase, until cruise flight level is reached. The aircraft is A320 and it is supposed that its mass is 64000 kg.

6.4.1 Meteorological data

Meteorological data are RAP data of April 3rd 2013 at about 01 p.m (UTC) (available in http://motherlode.ucar.edu:8080/thredds/catalog/fmrc/NCEP/RAP/CONUS_20km/files/c atalog.html). Wind speed and direction at altitude equal to about 5000 m are depicted in the following figure (Fig. 27).



Fig.27 The Wind speed, direction (arrows) and intensity (more colors) at 5000 m

6.4.2 Route and aircraft emissions

In the following table are reported the starting and ending points of the climb phase of the considered trajectory.

	Start Lat	Start	Start Alt	End Lat	End Lon	End Alt
	(°)	Lon (°)	(m)	(°)	(°)	(m)
climb	26.08	-80.114	457	28.43	-81.009	11278

Table 13 Initial and final position aircraft position

In order to compute noise emissions, we set two observation points for the climb phase (25.789N -80.2263E) and (26.0105N -80.1777E).

The real trajectory is taken from "FlightAware" website (http://flightaware.com).

In the following figure (Fig.3) the "normal" trajectory (in this case the trajectory of April 3rd 2013 at about 01 p.m.) (blue) and the trajectory of April 4th 2013 (black) are depicted, related to real cloud reflectivity the April 3rd 2013 at about 01 p.m.



Fig.28 Two trajectories performed by NKS724 in different days and atmospheric conditions are reported

In the following tables, emissions of the aircraft are reported. In table 14 the estimated emissions of the trajectory in different atmospheric conditions are reported. In particular, are calculated the emissions associated to the same trajectory with the real meteorological conditions and the ones forecasted one, three and six hours before, in order to assess the impact of meteorological conditions on the emissions.

NKS724	Real	1 h	3 h	6 h
	meteo	forecast	forecast	forecast
CO2 (kg)	5366	5415	5423	5407
NOx (kg)	62.99	63.76	63.98	63.63
Noise	53.33	54.18	54.03	54.93
(dB)				

Table 14 estimated emissions of NKS724 in different atmospheric conditions

The differences in the calculated emissions depend mainly on wind and cloud reflectivity values that are not so reliable for what concern the prediction [19]. On the other side, pressure, temperature, and humidity prediction are more reliable in few hour prediction [19]. Then, using the weighted Graph of the feasible trajectories, the emissions associated to different trajectories are calculated. In table 15 are reported the emissions associated to the real flight (column 2 in table 3) and the ones associated to optimized trajectories, applying Dijkstra mono or multi-object to select an optimized trajectory in accordance to different criteria (table 3, in column 3 Dijkstra Mono-objective CO2, 4 Dijkstra Mono-objective NOx, 5 Dijkstra Multi-objective). The multi-objective trajectory optimization is calculated attributing to NOx, CO2 and Noise emissions a weight of 0.4, 0.4, 0.2.

	FA emit	Dijkstra's algorithm			
		CO2	NOx	MO2	
CO2 (kg)	5366	5364	6249	5365	
NOx (kg)	62,99	107	54,41	56	
Noise (dB)	53.33	53,89	45,21	51.38	

Table 15 NKS724 emissions and emission associated to optimized trajectories

6.4.3 Comparison of emissions associated to optimized trajectory using Pareto

The optimization of more than one objective sets a problem on how to combine the single objectives in order to find a satisfactory solution. In the reported tests the three pollutants (CO2, NOx and Noise) were combined using a linear combination. Varying and combining the different weights it was possible to find a set of solutions "ordered" using the definition of Pareto optimal solutions often called Pareto Front.

This method was tested on the climb phase of the trajectory NKS724. The multi-objective function was computed using a linear combination of the three pollutants: CO2, NOx and Noise. The weights for each pollutant in the objective function used by Dijkstra's algorithm are between 0.0 and 1.0 with a step of 0.1 and the sum of the three weights must be one.

In the following table the solutions found using Dijkstra algorithm are reported. The first three columns report the weights used in the multi-objective function, the successive three columns report the value of the three pollutants computed. In the tables are underlined in green the solutions with minimum Noise and NOx emission, in cyan the solutions with minimum CO₂; in pink the solutions with minimum CO₂ for min NOX and Noise [32].

	Dijkstra's algorithm Pareto Front (climb NKS724)										
CO2 weight	NOx weight	Noise weight	CO2 emission	NOx emission	Noise Emission						
0,0	0,0	1,0	10922,48	168,44	39,70						
0,0	<mark>0,1-1,0</mark>	<mark>0,9-0,0</mark>	6249,07	<mark>54,41</mark>	<mark>45,21</mark>						
<mark>0,1-1,0</mark>	<mark>0,0-0,4</mark>	<mark>0,9-0,0</mark>	<mark>5345,86</mark>	107,48	<mark>53,89</mark>						
<mark>0,1-0,5</mark>	<mark>0,1-0,8</mark>	<mark>0,8-0,0</mark>	<mark>5364,82</mark>	<mark>88,10</mark>	<mark>51,68</mark>						
0,1	0,6-0,9	0,3-0,0	5425,02	78,24	55,72						

Table 16 Emissions associated to multi-object Djikstra optimized trajectories fordifferent set of emission weights

In the selected case the Minimum Noise emission is connected to the minimum NOx emission (generally both are minimized in case of constant engine regime). On the contrary Fuel consumption (and CO₂ that is proportional by a factor of 3.18) are minimized when NOx and Noise increase.

It is possible to identify some cases (underlined in pink in table 4) in which there is a limited emission of CO₂ (fuel consumption) in correspondence of low emission of NOx and Noise. Generally, the decision maker (i.e. the flight company) chooses the trajectory emission index and the weights and the criteria to be used to optimize the trajectory. In case the weather prediction (RAP) are not available, it is possible to use ISA standard model to calculate the emissions associated to the trajectory. In the following paragraph are reported and compared the emissions, associated to the real trajectory of NKS724, calculated with different atmospheric information (RAP, ISA RAP without wind) [32].

6.4.4 Comparison of pollutant emissions using different atmospheric information RAP (real weather data), ISA data and RAP without wind

When real atmospheric data are not available, it is possible to use ISA standard data to calculate trajectory emissions.

In each of the following tables, the values of pollutions emissions for each mono-objective optimized trajectory (Opt CO₂, Opt NO_x and Opt Noise) are reported with the different percentages respect real weather data. In each table, the third, the fourth and the fifth column identify the optimal trajectory minimizing a specific pollutant (for instance, OptCO₂ is the optimal trajectory computed using Q-AI minimizing CO₂). In the third, the fourth and the fifth row there are the pollutant emissions for each trajectory computed using RAP data. In the subsequent three rows, there are the emissions computed using ISA formulas and in the last three rows the emissions computed using RAP without wind [32].

	NKS 724 Climb phase									
		Opt CO2	Opt NOx	Opt Noise						
	CO2 (Kg)	5345	6249	10922						
RAP	NOx (Kg)	107.47	54.4	168.4						
	Noise (dB)	53.8	45.2	39.6						
	CO2 (Kg)	5219 (-2%)	6066 (-2%)	7322 (-32%)						
ISA	NOx (Kg)	87.8 (-18%)	51.1 (-6%)	85.7 (-49%)						
	Noise (dB)	72.5 (+25%)	59.9 (+24%)	57.9 (+31%)						
RAP	CO2 (Kg)	5234 (-2%)	6057 (-3%)	7330 (-32%)						
without wind	NOx (Kg)	105.2 (-2%)	54 (-0,7%)	99.4 (-32%)						
	Noise (dB)	72.5 (+25%)	59.9 (+24%)	57.9 (+31%)						

Table 17 Emissions associated to mono-object (CO2, NOx, Nose) optimizedtrajectories calculated with real weather condition (from RAP), ISA standardatmospheric condition and RAP data without wind

From the results, one can note that sometimes the optimal trajectory computed using RAP data is not optimal if emissions are computed using ISA formulas or RAP without wind. Moreover, the CO₂ and NO_x emissions computed using ISA formulas are less than the emission computed using RAP data. On the contrary, the noise emissions are greater when computed using ISA formulas. The emissions computed with ISA data and RAP without wind are very similar. This proves that wind has a big impact on pollutant emissions.

6.5 Data validation in X-plane flight simulator

The optimized trajectories have been validated in a X-plane flight simulator (Fig. 3,4) in which the correct models of A320 and engines were selected, the trajectories were uploaded in the FMS (flight management system) and the real Grib file contained the considered RAP file was uploaded in the simulation. In this way, it was possible to verify that the aircraft was following the optimized trajectory in the proper way, with little deviations.



Fig.29 X-plane flight simulator in which is visible the selected aircraft (A320) flight along the optimized trajectory (in pink in the picture) uploaded in FMS.



Fig.30 X-plane flight simulator cockpit view of the selected A320

The X-plane flight simulator was connected by Ethernet LAN to MARS in weather radar mode simulation (Fig.5), in which it was uploaded the considered weather situation. In this way, it was possible to see the aircraft moving along the trajectory uploaded on the FMS and the weather reflectivity evolving coherently with the aircraft movement. When the weather radar detects the unforeseen weather event (weather reflectivity) it sends this information to the trajectory optimized that automatically updates the graph of feasible trajectories, generates an optimized trajectory and it sends it to the FMS, so the aircraft begins to follow the new updated trajectory.



Fig.31 MARS weather radar simulator display in which the cloud reflectivity is visualized

CHAPTER 7 MINIMUM SIZE GRAPH GENERATION AND RESULTS

In this section is described our approach to automatically generate a minimum size graph of trajectories to guarantee feasible acceptable solutions in a minimum computational time. This approach is useful to run the trajectory optimizer on onboard computer that have limited performances a process capacities. In the following paragraphs, will be detailed the graph generation method and it will be underlined how the graph generation is different for the different phases of flight. In particular, for the cruise phase are important the position (latitude and longitude) variation while the altitude and speed variations are less important, while in the climb and descent phase are more important the altitude and speed variations. For the optimized trajectories, the climb and cruise phases are considered, because they are the only ones in which it is possible to obtain a relevant decrease of fuel consumption and emissions, while in descent phase generally the pilot perform a continuous descent approach with the engine in idle mode, so there are no big margins of possible improvements.

7.1 Automatically Graph Generation

The construction procedure of the graph of feasible trajectories (base of data of our optimizer) is the one described in par. 5.1.5. This procedure is automatized generating, in a recursive way, graphs starting from very low resolution ones, that don't provide feasible

solutions, and increasing the graph resolution till feasible solutions are available. So the suggested method is based on recursive graphs generation that stops where suitable stop criteria are reached. To optimize the graph generation process, these stops criteria, as it will be shown later, is applied to a different DXi depending on the phase of flight.

In general, the chosen stop criteria of the graph generation are:

- DXi reached selected thresholds depending on the phase of flight;
- The fuel consumption doesn't increase anymore for 3 consecutive steps
- The mean and mode of the maximum and minimum DXi (depending on phase of flight) doesn't increase for 3 consecutive steps.

To demonstrate the suggested procedure, several tests have been performed in Matlab. So, several matlab programs have been implemented to automatically generate the minimum graphs (for a selected accuracy) of the feasible trajectories for an A320 in climb and cruise phase. The parameters automatically varied (till some stop criteria are reached) in such matlab programs, are the minimum, maximum and step of 4 of the 5 parameters the identified the nodes (latitude, longitude, altitude, and speed). The 5st parameter (heading step) is fixed to 60° because we have a graph based on concentrated parameters, so each waypoint identifies a different aircraft state.

7.2 Experimental set up

To demonstrate the proposed method, four use cases have been considered, in particular, 2 trajectories in cruise and 2 in climbs phase. Two of this use cases are identified the same aircraft and trajectory considered in cap. 6, in particular, the test case 1 and the test case 2. The method was successfully applied to the 4 use cases and the results are reported in the following chapters.

7.2.1 Test cases characterization

In all the 4 cases the aircraft considered is an A320 and we suppose that during the flight the mass of the aircraft is 64000 kg.

The flights are taken from real word (from flightaware) and the considered trajectories begin and end the positions (considered state points) listed in the following table. Initial states:

phase of flight	x0[degrees]	y0[degrees]	z0[m]	Vtas0[m/s]	heading0[degrees]
climb test3	40.86	-112.616	5882	197	260

climb test case 2	44.8258	-93.2317	945	105	214
cruise test case 1	35.35	-99.4642	10673	228	99
Cruise test4	40.5753	-114.38	10363	232.4	260

Table 18 Initial waypoint position, speed and heading for the analyzed test casesFinal states are:

phase of flight	xf[degrees]	yf[degrees]	zf[m]	Vtasf[m/s]	headingf[degrees]
climb test3	40.6036	-114.21	10363	233	260
climb test2	44.11	-95.8472	10973	238	286
cruise test1	35.4783	-94.3931	10668	225	89
cruise test4	40.2611	-116.1	10363	233.8	260

Table 19 Fina	l waypoint	position,	speed and	heading for	the analyzed	test cases
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7.2.1.1 Test cases 3

An A320, in climb phase, is flying from Salt Lake City an Oakland (DAL1253). The initial point for the optimized trajectory is (40.86 N - 112,6164 E) at 5882 m altitude, while the final waypoint is (40.6036 N - 114.2131 E) at an altitude of 10363 m (150 Km far away). The initial speed is 197 m / s and the final speed is 233 m / s and the heading is 260°. The aircraft is A320 and it is supposed that its mass is 64000 kg.

In the following table are reported some examples of results for the calculation of graphs with different resolution in latitude and longitude (Delta_X), altitude (Delta_Z), speed (Delta_V and the results associated to the different optimization objectives (Multi-objective MO, NOx, time and Fuel).

Delta_X m	20000	20000	30000	30000	20000	30000
Delta_Z m	600	700	700	600	600	600
Delta_H deg	45	45	45	60	45	45
Delta_V m/s	12	12	12	12	20	20
Atmosphere	ISA	ISA	ISA	ISA	ISA	ISA
Compute time	1363	1075	163	109	778	99
archs	2928430	2305700	345716	220884	1521151	220884

Emiss time	171	134	20	13	90	10
Fuel_MO (Kg)	722	728	703	708	723	711
NOx	16	15	15,9	15	16	16
Time	764	764	731	731	745	729
Fuel_time (Kg)	700	703	723	730	728	718
NOx	17	17	18	18	18	18
Time	648	648	645	645	678	649
Fuel_NOx (Kg)	700	701	710	711	698	714
NOx	15	15	15	15	16	15
Time	723	717	731	731	709	729
Fuel_Fuel (Kg)	689	688	693	692	697	699
NOx	16	16	16	16	16	16
Time	689	676	692	682	696	691

Table 20 Graph computation with different resolution and emissions associated to the trajectory optimized with different optimization objectives.

7.2.1.2 Test cases 2 Graph generation

Refer to chapter 6.3 for the characteristics of this flight.

In the following table are reported some examples of results for the calculation of graphs with different resolution in altitude (Delta_Z), and the results associated to the different optimization objectives (Multi-objective MO, NOx, time and Fuel).

Delta_X m	40000	40000	40000	40000	40000	40000
Delta_Z m	800	970	1050	1200	1300	3330
Delta_H deg	45	45	45	45	45	45
Delta_V m/s	30	30	30	30	30	30
Atmosphere	ISA	ISA	ISA	ISA	ISA	ISA
Compute time	1180	851	722	623	502	173
archs	312975	2268335	1896243	1560512	1225409	361025
Emiss time	220	160	135	114	86	25

Fuel_MO (Kg)	1373	1380	1384	1377	1381	1371	
NOx	34	34	34	34	34	35	
Time	1189	1189	1189	1187	1216	1211	
Fuel_time (Kg)	1509	1366	1537	1458	1483	1638	
NOx	45	39	46	44	45	52	
Time	1049	1031	1061	1049	1049	1061	
Fuel_NOx (Kg)	1546	1547	1548	1547	1433	1548	
NOx	33	33	33	33	33	33	
Time	1488	1488	1488	1488	1297	1488	
Fuel_Fuel (Kg)	1345	1341	1362	1355	1355	1364	
NOx	36	36	35	35	35	36	
Time	1124	1124	1158	1156	1156	1134	

 Table 21 Graph computation with different resolution and emissions associated to the trajectory optimized with different optimization objectives.

7.2.1.3 Test cases 1 Graph generation

In the following table are reported some examples of results for the calculation of graphs with different resolution in latitude and longitude (Delta_X), and altitude (Delta_Z), and the results associated to the different optimization objectives (Multi-objective MO, NOx, time and Fuel).

Delta_X m	20000	25000	30000	30000	20000	40000	
Delta_Z m	150	500	500	500	1000	500	
Delta_H deg	45	45	45	45	45	45	
Delta_V m/s	1,4	1,4	1,4	2	1,4	1,4	
Atmosphere	ISA	ISA	ISA	ISA	ISA	ISA	
Compute time	1400	290	150	72	140	45	
archs	4872622	871035	447046	<mark>219358</mark>	367910	146868	
Emiss time	170	46	20	9	14	7	
Fuel_MO (Kg)	1139	1139	1090	1091	1157	1144	

NOx	58,8	58,8	51,8	51,8	59,3	58,9
Time	680	680	679	679	680	681
Fuel_time (Kg)	1149	1149	1094	1095	1160	1152
NOx	59,4	59,4	59,4	59 <i>,</i> 4	59,7	59,5
Time	649	649	649	651	649	650
Fuel_NOx (Kg)	1129	1129	1090	1094	1100	1109
NOx	50,8	50,8	50,8	50 <i>,</i> 8	52,3	54,9
Time	680	680	679	679	680	677
Fuel_Fuel (Kg)	1090	1091	1090	1090	457	444
NOx	52,9	52,9	51,8	51.8	59,3	59
Time	669	669	679	679	680	680

Table 22 Graph computation with different resolution and emissions associated to the trajectory optimized with different optimization objectives.

7.2.1.4 Test cases 4

In the following table are reported some examples of results for the calculation of graphs with different resolution in latitude and longitude (Delta_X), and altitude (Delta_Z), and the results associated to the different optimization objectives (Multi-objective MO, NOx, time and Fuel).

Delta_X m	20000	25000	30000	30000	20000	40000	
Delta_Z m	150	500	500	500	1000	500	
Delta_H deg	45	45	45	45	45	45	
Delta_V m/s	1,4	1,4	1,4	1,4 2		1,4	
Atmosphere	ISA	ISA	ISA	ISA	ISA	ISA	
Compute time	1390	274	128	62	127	43	
archs	4872622	871035	447046	219358	367910	146868	
Emiss time	166	29	15	7	12	5	
Fuel_MO (Kg)	419	419	420	421	437	424	
NOx	6,8	6,8	6,8	6,8	7,3	6,9	
Time	667	667	666	666	667	664	

Fuel_time (Kg)	429	429	430	429	440	432
NOx	7,4	7,4	7,4	7,4	7,7	7,5
Time	636	636	636	638	636	637
Fuel_NOx (Kg)	419	419	420	421	437	424
NOx	6,8	6,8	6,8	6,8	7,3	6,9
Time	667	667	666	666	667	664
Fuel_Fuel (Kg)	418	418	420	421	437	424
NOx	6,9	6,9	6,9	7	7,3	7
Time	656	656	656	656	667	657

Table 23 Graph computation with different resolution and emissions associatedto the trajectory optimized with different optimization objectives.

7.2.2 Computational Method applied

As described in the previous section, to generate and identify the more suitable graph, of feasible trajectories, to reduce the computational time for the trajectory optimization, we started from a very small graph and we varied Ximax, Ximin, DXi (for i = 1 to 4), where Xi are the aircraft altitude, speed and then latitude and longitude, till the automatic graph generation met the stop criteria mentioned before.

The initial graph has different DXi resolution depending on the phase of flights (in the climb phase the altitude and speed variations should be more refined and we varied them with smallest steps respect longitude and latitude variations, while in cruise phase longitude and latitude steps are thinner and altitude and speed are variations are less important because are almost constant).

In particular, for the cruise phase the initial graph has a bigger resolution for latitude and longitude and smaller resolution for speed and altitude, because in this phase of flight the altitude and the speed depend on the flight level of the civil airspace and from the aircraft dynamic, and we need a higher latitude and longitude resolution to allow possible aircraft manoeuvre to avoid no flight zones.

For the climb phase the initial graph will have a higher resolution in altitude and in speed to allow the aircraft to reach the final values of the altitude and speed.

The tests were performed in the following way:

- Recursive graph calculation varying the following variables:

- Max and Min altitude (such values were chosen based on maximum cruise level feasible or free flight levels)
- o Altitude steps
- o Max speed, min speed
- o Speed steps

The chosen graphs generation stop conditions were the followings:

- o Minim fuel consumption for the same number of waypoints
- \circ Altitude and speed steps resolution (ex. speed< k1 m/sec; altitude < k2 m)

For what concern the cruise phase we fixed the initial graph with a certain number of points in latitude and longitude and less points in speed and altitude, because the cruise altitude depends on the assigned flight level and the speed depends on the rules of flight in the civil airspace and on the aircraft flight dynamic. It could be necessary to turn the aircraft to avoid the no flight zones, so it is required to have a high resolution in latitude and longitude.

7.2.3 Software implementation

The software is implemented in Matlab, and in the following block scheme are represented the step implemented.



Fig.32 Block scheme of the software implementation

In the first step the Test case is selected, and a table of the grid values (altitude, speed) is generated. Then the graph is generated from the table saved. Later the results (emissions, etc.) are evaluated and the stop criteria are checked. If stop criteria are reached, an exel file contained all the results is saved, if not the process start again with another iteration. In the following table is reported an example of the exel file generated by the program:

											num		num	
											Punti	Fuel	Punt	num
	minAlt	maxAlt	deltaAlt							tempo_ese	Traiett	Consupti	iQuo	Punti
iteraz	[m]	[m]	[m]	moda	vmin	vmax	deltaV	vmedia	vmoda	cuzione	oria	on	ta	Vel
1	8000	9000	1000	8000	170	200	30	170	170	1.1001733	1	0	2	2
2	8000	9000	1000	8000	200	230	30	200	200	1.07607134	1	0	2	2
3	8000	9000	1000	8000	230	260	30	230	230	1.10981232	1	0	2	2
4	9000	10000	1000	9000	170	200	30	170	170	1.14838325	1	0	2	2
5	9000	10000	1000	9000	200	230	30	200	200	1.11712377	1	0	2	2
6	9000	10000	1000	9000	230	260	30	230	230	1.03400782	1	0	2	2
7	10000	11000	1000	10000	170	200	30	170	170	1.13460296	1	0	2	2
8	10000	11000	1000	10000	200	230	30	200	200	1.10780574	1	0	2	2
9	10000	11000	1000	11000	230	260	30	230	230	3.16672524	5	1400	2	2
Tempo														
calcolo														
tabella	11.995	0	0	0	0	0	0	0	0	0	0	0	0	0
10	10000	10500	500	10000	230	245	15	245	245	1.13614594	1	0	2	2
11	10000	10500	500	10000	245	260	15	245	245	1.11033077	1	0	2	2
12	10500	11000	500	11000	230	245	15	232.14	230	3.75608512	7	1369	2	2
13	10500	11000	500	11000	245	260	15	245	245	3.45225489	7	1360	2	2
Tempo														
calcolo														
tabella	9.4548	0	0	0	0	0	0	0	0	0	0	0	0	0
14	10500	10750	250	10500	245	252.5	7.5	245	245	1.07074204	1	0	2	2
15	10500	10750	250	10500	253	260	7.5	252.5	252.5	1.17156262	1	0	2	2
16	10750	11000	250	11000	245	252.5	7.5	245	245	3.63564961	7	1355	2	2
17	10750	11000	250	11000	253	260	7.5	252.5	252.5	3.68230985	7	1359	2	2
Tempo														
calcolo														
tabella	9.5603	0	0	0	0	0	0	0	0	0	0	0	0	0
18	10750	10875	125	10750	245	248.8	3.75	245	245	1.13139279	1	0	2	2
19	10750	10875	125	10750	249	252.5	3.75	248.75	248.75	1.12329215	1	0	2	2
20	10875	11000	125	11000	245	248.8	3.75	245	245	3.91158873	7	1358	2	2
21	10875	11000	125	11000	249	252.5	3.75	248.75	248.75	3.59950745	7	1359	2	2
Tempo														
tabella	0 7659	0	0	0	0	0	0	0	0	0	0	0	0	0
22	9.7056 10975	10020	62 5	10075	245	246.0	1 075	245	245	1 09524726	1	0	2	2
22	10875	10938	62.5	10875	245	246.9	1.875	245	245	1.08534726	1	0	2	2
23	10875	10938	62.5	10875	247	248.8	1.875	246.88	246.88	1.15503894	1	0	2	2
24	10938	11000	62.5	11000	245	246.9	1.8/5	245	245	3.77456513	/	1355	2	2
25	10938	11000	62.5	11000	247	248.8	1.875	246.88	246.88	3.69944612	7	1355	2	2
calcolo														
tabella	9,7144	0	0	n	0	0	0	n	0	n	0	0	0	0
Tempo	5.7 211				Ŭ	ľ	Ŭ	Ű	ľ	ů			Ŭ	
totale	50.49	0	0	0	0	0	0	0	0	0	0	0	0	0

Table 24 Exel file generated by the Matlab program for the automatic grid generation in which all useful parameters are contained.

In the exel file are saved all the parameters useful for the graph generation and evaluation. In particular:
- The number of iterations
- The Min, Max and delta of the varied parameters (altitude, speed, etc.)
- The Mean and Mode of the parameters varied
- The computational time
- The waypoints associated to the trajectory
- The fuel consumption
- The points associated to the discretised parameters.

7.3 Tests Results

For each of the 4 use cases, two simulations with 3 and 2 nodes were performed. In the following table are reported the obtained Node and Arch of the graphs, for the better solution, the related emissions the algorithm iterations and the computational time.

Test case	Archs	Fuel (kg)	Iterations	Computational time (Sec)
Test case 3	332114	693	30	82
Test case 2	130580	1355	25	50
Test case 1	12500	1090	20	3
Test case 4	10200	420	20	2.8

Table 25 Test cases results in term of graph dimension, computational time, iterations, and trajectory emissions

Comparing the results obtained in the previous paragraphs with the ones contained in the Table 24 it is possible to verify that for almost the same fuel consumption and graph accuracy the computational time is much less (2 time less in test case 3, 3 time less in test case 2 and almost 10 time less in test case 1 and 4).

For what concern the tests in climb phase, as mentioned before, we must manage a big change in speed and altitude, so the selected steps in speed and altitude are quite thin (ex. (Vf-Vi)/8; (Hf-Hi)/8); while there is a little change in position, so the steps in latitude and longitude have less influence on the computational time.

For what concern the tests in cruise phase, the speed and altitude are almost fixed, so we choose only one or two steps, while we have to manage a big change position, and we need thin steps in latitude and longitude (ex. (Xf-Xi)/8).

Comparing the different parameters values (min altitude, max altitude, step altitude, emissions, computational time, etc.), for what concern the tests in cruise phase, it was possible to establish that the better solution, in the test case 1, was the one performed with 2

nodes simulation since all the parameters values were the same for the minimum computational time. In the test 4 use case the results are almost the same for 2 and 3 nodes, and the computational time is very low in both cases. For what concern the tests in climb phase, to reach a suitable solution, and obtain a graph able to cover all the foreseen range in altitude and speed, are required more nodes, interactions, and computational time.

The previous calculation where performed in a portable workstation with the following characteristics:

- Operating System: Genuine Windows 7 Professional 64
- Processor: 3rd Generation Intel® CoreTM i7 Quad-Core1
- Memory: DDR3 SDRAM PC3-12800, 1600 MHz, dual-core processors support 2 memory slots, 2/4/8 GB16 SODIMMs
- Internal Storage: 320/500/750 GB 7200 rpm HDD, 500 GB 7200 rpm SED (Self Encrypting Drive), SATA 6 Gb/s, 128/180 GB SSD
- Graphics: NVIDIA Quadro K2000M, with 2 GB dedicated DDR3 video memory

For the considered test cases, the computational time is suitable for on-board application, since the available time is around 5 minutes and the obtained computational time is less than 50 seconds. The proposed method allows to generate an adaptive grid in the minimum time with a low dimension for the required accuracy. These graphs have been compared with big graphs, in terms on emissions, graph dimension, arches, computational time. These graphs allow minimum memory/space occupancy and minimum computational time.

When the computational time is not acceptable for on-board applications, other graph generation strategies should be applied, like to generate set of smaller graphs connected together in the interested space. That would drastically decrease the computational times and allow an on-board real time trajectory optimization.

CHAPTER 8 CONCLUSIONS

In the present thesis, important problems for the aircraft flight have been taken into account and the possible solutions have been proposed. The problems described are the necessity for the aircraft to avoid bad weather conditions and to the reduce the fuel consumption and the pullant emissions. The proposed solution is a graph based on-board multi-object trajectory optimizer.

In the first part of this thesis is provide an overview of the weather phenomenon dangerous for the aircraft flight and an overview of avionic instruments and information sources that can provide weather information to the pilot. Then an overview on civil aircraft flight in terms of aircraft categories, performed trajectory and phase of flight is provided to contextualize the object of the proposed optimization (aircraft trajectory for different phases of flight). Later an overview of the available trajectory optimization algorithms and methods is provided and some performance comparison is described. The next chapter report the description of our approach for the multi-object aircraft trajectory optimization for weather avoidance and emission reduction. The algorithm proposed is Dijkstra for the generation of the graph of feasible trajectories in a certain volume of space. Such graph is valid for a certain aircraft of which is available the performance model, in a certain airspace volume, in which are available the atmospheric conditions. For this reason, are taken into account and described the model used to generate the graph, in particular the aircraft, emission, weather and engine models. In the next chapter, some results for a typical civil aircraft (A320) are provided and the fuel consumption of the optimized trajectories are compared with the real trajectory performed by the aircraft and downloaded from "flightaware" database. The obtained results are quite interested because show a significant fuel and emission reduction possibility, while avoiding bad weather conditions, respect the real flight. In this chapter is also shown how much unreliable are the weather predictions, in particular, the weather

reflectivity and the wind, and that justify why an on-board trajectory optimizer would be very useful. Unfortunately, on-board there are avionic devices with limits in performances and in computational time. For this reason, finally it is proposed an innovative method to automatically generate a graph of trajectories (to be used as base of data for the trajectory optimizer), with minimum size and computational time suitable for on-board applications, and some interesting result is provided. The proposed method identifies a process to automatically generate the better graphs, for the trajectory optimizer, in terms minimal dimension and computational time, so suitable for on-board application integrated in a decisional support system. The possible on-board devices target for such a decision support system are EFB (Electronic Flight Bag) or tablet.

Acronyms

AAC	Airline Administrative Control	
ACARE	Advisory Council for Aeronautics Research in Europe	
ACARS	Aircraft Communications and Reporting System	
AOC	Aircraft Operational Control	
ATC	Air Traffic Control	
A-WXR	<u>A</u> dvanced <u>W</u> eather <u>R</u> adar	
dB	<u>D</u> eci <u>B</u> el	
BADA	Base of Aircraft DAta	
CAT	clear air turbulence	
deg	<u>deg</u> ree(s)	
DO	<u>DO</u> cument	
DOW	Description Of Work	
DSS	<u>D</u> ecision <u>S</u> upport <u>S</u> ystem	
EEC	Eurocontrol Experimental Centre	
EFB	Electronic Flight Bag	
FAA	Federal Aviation Administration	
FMS	<u>F</u> light <u>M</u> anagement <u>S</u> ystem	
GRIB	Gridded Binary Data files (General Regularly-distributed Information in Binary form)	
GRUMP	Global Rural-Urban Mapping Project,	
ICAO	International <u>C</u> ivil <u>Aviation</u> <u>Organization</u>	
ICD	Interface Control Document	
ID	IDentification	
ISA	International Standard Atmosphere	
ITD	Integrated Technology Demonstrator	
JTI	Joint <u>T</u> echnology <u>I</u> nitiative	

JU	Joint Undertaking	
°К	Kelvin Degrees	
kg	kilogram(s)	
LAN	Local <u>A</u> rea <u>N</u> etwork	
М	Mach Number	
m	meter(s)	
m ²	square <u>m</u> eters	
m/s	meter(s) per second	
METAR	METeorological Aerodrome Report.	
MFD	<u>M</u> ulti <u>F</u> unctional <u>D</u> isplay	
MMI	Man Machine Interface	
МО	Meteorological Office	
МТМ	Management of Trajectory and Mission	
NAS	National Airspace System	
NASA	National Aeronautical and Space Administration	
NASDAC	National Aviation Safety Data Analysis Center	
NEM	Noise Evaluation Module	
NOAA	National Oceanic and Atmospheric Administration	
NOx	<u>N</u> itrogen <u>O</u> xides	
NOTAM	NOTice to <u>A</u> ir <u>M</u> en	
NPD	Noise Power Distance	
NTSB	National Transportation Safety Board	
NWP	Numerical Weather Prediction	
Ра	Pascal	
Q-AI	Quasi <u>A</u> rtificial <u>I</u> ntelligence	
RAP	Rapid Refresh	
RTCA	Radio Technical Commission for Aeronautics	
RUC	Rapid Update Cycle	
SESAR	<u>S</u> ingle <u>E</u> uropean <u>S</u> ky <u>A</u> TM <u>R</u> esearch	
sec	second(s)	
SEL	<u>S</u> ound <u>E</u> xposure <u>L</u> evel	
SGO	Systems for Green Operations	
TAF	Terminal <u>A</u> rea <u>F</u> orecast	

ТМ	<u>T</u> rajectory <u>M</u> anagement	
UDP	User Datagram Protocol	
WAFC	World Area Forecast Centres	
WP	Work Package	
WXR	Weather Radar	

Acronyms

References

- [1] ACARE, European Aeronautics A Vision for 2020 Report of the Group of Personalities, January 2001
- [2] ACARE, Strategic Research Agenda 1, October 2002
- [3] ACARE, Strategic Research Agenda 2, October 2004
- [4] D. Michalek and H. Balakrishnan, Identification of Robust Routes using Convective Weather Forecasts, 8th USA/Europe Air Traffic Management R&D Seminar, Napa Valley, CA, June/July 2009.
- [5] M. Rubnich and R. DeLaura, An Algorithm to Identify Robust Convective Weather Avoidance Polygons in En Route Airspace, AIAA Aviation Technology, Integration, and Operations (ATIO) Conference 13 - 15 September 2010, Fort Worth, Texas.
- [6] M.H. Nguyen, S. Alam, J. Tang, and H. Abbass, Ants-inspired dynamic weather avoidance trajectories in a traffic constrained enroute airspace; 6th EUROCONTROL Innovative Research Workshop & Exhibition, 12- 2007, pp. 205–212.
- [7] The Potential Impacts of Climate Change on Transportation- Gloria Kelusa
- [8] Climatology manual for Airline Pilots H.R. Quantick FRAeS, FRMetS
- [9] Panel on Atmospheric Effects of Aviation and Board on Atmospheric Sciences & Climate and Commission on Geosciences & Environment & Resources and National Research Council, Atmospheric Effects of Aviation: A Review of NASA's Subsonic Assessment Project, 1999
- [10] WMO Publication No: 306, Manual on Codes, Volume 1.2, Part B Binary Codes
- [11] http://nomads.ncdc.noaa.gov
- [12] Oxford Aviation Training, Jeppesen, (2002), "JAA Airline Transport Pilot's Licence, Theoretical Knowledge Manual, 022 INSTRUMENTATION" Second Edition, First Impression, Osford Aviation Services Limitet 2001, England.
- [13] Oxford Aviation Training, Jeppesen, (2002), "JAA Airline Transport Pilot's Licence, Theoretical Knowledge Manual, 050 METEREOLOGY" Second Edition, First Impression, Osford Aviation Services Limitet 2001, England.
- [14] Colella G., (2009), "Meteorologia Aeronautica", V Ed., IBN Editore, Roma
- [15] Trebbi R., (2012), "Meteorologia per Piloti", Aviabooks Editore (La Bancarele Aeronautica), Milano
- [16] Moir I., Seabridge A., (2008), "Aircraft System", Third Edition John, Wiley & Sons Ltd., England, Pag. 441-493
- [17] Diston D.J., (University of Manchester), (2009), "Computational Modelling and Simulation of Aircraft and the Environment", First Edition John, Wiley & Sons Ltd., England.
- [18] Yiyuan Zhao and Rhonda a. Slattery. Capture conditions for merging trajectory segments to model realistic aircraft descents. Journal of Guidance, Control, and Dynamics, 19(2):453{460, March 1996.
- [19] G. Serafino, M. Bernabò, S. Mininel, G. Stecco, M. Nolich, W. Ukovich, G. Pedroncelli, M. P. Fanti, "Effects of weather condition on aircraft emissions in climb phase", Digital Avionics Systems Conference (DASC), Williamsburg, VA, USA, pp. 3A6-1 3A6-12, October 2012.
- [20] Baughcum, S.L., T. G. Tritz, S. C. Henderson, D. C. Pickett, 1996, Scheduled Civil Aircraft Emissions Inventories for 1992: Database Development and Analysis, Appendix D: Boeing Method 2 Fuel Flow Methodology Description, Report NASA CR 4700, The Boeing Company
- [21] Nuic, A., 2012, User Manual for the base of AircraftData (BADA) Revision 3.10, Eurocontrol

- [22] Experimental Center.International Civil Aviation Organization (ICAO). ICAO Engine Exhaust Emissions Databank, Issue 15-B, 2007.
- [23] EUROCONTROL Experimental Center, The Advanced Emission Model (AEM3) Version 1.5 Validation Report; EEC/SEE/2004/004
- [24] Airbus A-320 POH: Pilot's Operating Handbook", http://www.despair.ch/staff/library/thc003.pdf
- [25] AIRBUS, "A318/A319/A320/A321 Flight deck and systems briefing for pilots", Ref. STL 945.7136/97 – Issue 4, 2007
- [26] M.P. Fanti, S. Mininel, M. Nolich, G. Stecco, W. Ukovich, M. Bernabò and G. Serafino, Flight Path Optimization for Minimizing Emissions and Avoiding Weather Hazard, ACC, 06/2014
- [27] ICAO, ICAO Engine Exhaust Emissions Databank, Issue 15-B, 2007.
- [28] ICAO, "Environmental report 2010," 2010.
- [29] R. K. Ahuja, T. L. Magnanti, and J. B. Orlin. Network flows: Theory, Algorithms, and Applications. Prentice-Hall, NJ, 1993
- [30] G. SERAFINO, MULTI-OBJECTIVE TRAJECTORY OPTIMIZATION TO REDUCE AIRCRAFT EMISSIONS IN CASE OF UNFORESEEN WEATHER EVENTS, 29TH ICAS 2014 CONFERENCE, ST. PETERSBURG, 7-12 SEPTEMBER 2014
- [31] ECAC.CEAC Doc 29, Report on Standard Method of Computing Noise Contours around Civil Airports, Volume 1: Application guide, 2005.
- [32] EFFECTS OF WEATHER CONDITION ON AIRCRAFT EMISSION IN CLIMB PHASE, MESAS 2015 CONGRESS, PRAGUE, 29-30 APRIL 2015, G. SERAFINO, Springer
- [33] G. SERAFINO, ONBOARD TRAJECTORY OPTIMIZATION FOR WEATHER AVOIDANCE AND EMISSION REDUCTION, GREENER AVIATION, 3AF, BRUXELLES, 11-13 OCTOBER 2016
- [34] David H. Jacobson, David Q. Mayne. "Differential Dynamic Programming" Elsevier, 1970.
- [35] Patterson, Michael A.; Rao, Anil V. (2014-10-01). "GPOPS-II: A MATLAB Software for Solving Multiple-Phase Optimal Control Problems Using hp-Adaptive Gaussian Quadrature Collocation Methods and Sparse Nonlinear Programming". ACM Trans. Math. Softw. 41 (1): 1:1–1:37. doi:10.1145/2558904. ISSN 0098-3500.
- [36] Waitz, I., J. Townsend, J. Cutcher-Gershenfeld, E. Greitzer, J. Kerrebrock, 2004, Aviation and the environment: Report to the United States Congress, Partnership for Air Transp. Noise and Emissions Reduction, MIT, Cambridge.
- [37] Nuic, A., 2012, User Manual for the base of Aircraft Data (BADA) Revision 3.10, Eurocontrol Experimental Center.
- [38] Dopelheuer, A., 2000, Aircraft emission parameter modeling, Air & Space Europe, 2, 34-37.
- [39] International Civil Aviation Organization (ICAO). ICAO Engine Exhaust Emissions Databank, Issue 15-B, 2007.
- [40] Baughcum, S.L., T. G. Tritz, S. C. Henderson, D. C. Pickett, 1996, Scheduled Civil Aircraft Emissions Inventories for 1992: Database Development and Analysis, Appendix D: Boeing Method 2 Fuel Flow Methodology Description, Report NASA CR 4700, The Boeing Company.
- [41] International Civil Aviation Organization (ICAO). ICAO Engine Exhaust Emissions Databank, Issue 15-B, 2007
- [42] The Advanced Emission Model (AEMIII), ver 1.5, Eurocontrol, Validation report, 2004
- [43] ECAC.CEAC Doc 29, Report on Standard Method of Computing Noise Contours around Civil Airports, Volume 1: Application guide, 2005.
- [44] Dopelheuer, A.,2000, Aircraft emission parameter modeling, Air & Space Europe, 2, 34-37.
- [45] International Electrotechnical Commission: Sound level meters. IEC 61672-1 (2002)
- [46] International Organization for Standardization: Acoustics Procedure for describing aircraft noise heard on the ground. ISO 3891 (1978). [This standard may be replaced or supplemented by a new standard that is currently in draft form as ISO/CD 20906 (2003): Unattended monitoring of aircraft sound in the vicinity of airports.]
- [47] International Organization for Standardization: Acoustics Description, measurement and assessment of environmental noise – Part 1: Basic quantities and assessment procedures. ISO 1996-1 (2001).
- [48] International Civil Aviation Organization: International Standards and Recommended Practices, Environmental Protection, Annex 16, Volume I, Aircraft Noise, 4th Edition, July 2005.

- [49] Eric Homan, Peter Martin, Thomas P• utz, Aymeric Trzmiel, and Karim Zeghal. Airborne Spacing: Flight Deck View of Compatibility with Continuous Descent Approach (CDA). Interface, 2007.
- [50] G.L. Slater. Study on variations in vertical profile for CDA descents aiaa-2007-7778, 2009. [9th AIAA Aviation Technology, Integration, and Operations Conference 21 23 September 2009].
- [51] John E. Robinson III Keenan Roach. A Terminal Area Analysis of Continuous Ascent Departure Fuel Use at Dallas/Fort Worth International Airport – aiaa, 2010. [10th AIAA Aviation Technology, Integration, and Operations (ATIO) Conference 13 - 15 September 2010, Fort Worth, Texas].
- [52] Francois Le Sellier. Discrete Real-Time Flight Plan Optimization. 1999.
- [53] W.a. Kamal and I. Postlethwaite. Real Time Trajectory Planning for UAVs
- [54] Using MILP. Proceedings of the 44th IEEE Conference on Decision and Control, 2005.
- [55] I. M. Ross and M. Karpenko, "A Review of Pseudospectral Optimal Control: From Theory to Flight," Annual Reviews in Control, Vol. 36, pp. 182-197, 2012.
- [56] Survey of Numerical Methods for Trajectory Optimization; John T. Betts Journal of Guidance, Control, and Dynamics 1998; 0731-5090 vol.21 no.2 (193-207)
- [57] Francois Le Sellier. Discrete Real-Time Flight Plan Optimization. 1999.
- [58] W.a. Kamal and I. Postlethwaite. Real Time Trajectory Planning for UAVs
- [59] Using MILP. Proceedings of the 44th IEEE Conference on Decision and Control, 2005.
- [60] Arthur Richards and Jonathan P How. Collision Avoidance Using Mixed Integer Linear Programming Hong Yang and Yiyuan Zhao. Trajectory Planning for Autonomous Aerospace Vehicles amid Known Obstacles and Conflicts. Journal of Guidance, Control, and Dynamics, November 2004.
- [61] John T. Betts "Practical Methods for Optimal Control and Estimation Using Nonlinear Programming" SIAM Advances in Design and Control, 2010.
- [62] Christopher L. Darby, William W. Hager, and Anil V. Rao. "An hp-adaptive pseudospectral method for solving optimal control problems." Optimal Control Applications and Methods, 2010.
- [63] Patterson, Michael A.; Rao, Anil V. (2014-10-01). "GPOPS-II: A MATLAB Software for Solving Multiple-Phase Optimal Control Problems Using hp-Adaptive Gaussian Quadrature Collocation Methods and Sparse Nonlinear Programming". ACM Trans. Math. Softw. 41 (1): 1:1–1:37. doi:10.1145/2558904. ISSN 0098-3500.
- [64] I. M. Ross and M. Karpenko, "A Review of Pseudospectral Optimal Control: From Theory to Flight," Annual Reviews in Control, Vol. 36, pp. 182-197, 2012.
- [65] Survey of Numerical Methods for Trajectory Optimization; John T. Betts Journal of Guidance, Control, and Dynamics 1998; 0731-5090 vol.21 no.2 (193-207)
- [66] Anil V. Rao "A survey of numerical methods for optimal control" Advances in Astronautical Sciences, 2009.
- [67] Camila C. Francolin, David A. Benson, William W. Hager, Anil V. Rao. "Costate Estimation in Optimal Control Using Integral Gaussian Quadrature Orthogonal Collocation Methods" Optimal Control Applications and Methods, 2014.
- [68] Lloyd N. Trefethen. "Approximation Theory and Approximation Practice", SIAM 2013
- [69] David H. Jacobson, David Q. Mayne. "Differential Dynamic Programming" Elsevier, 1970.
- [70] "Vertical wind shear. Retrieved on 2015-10-24".
- [71] Jump up to: a b c d Publishing, Integrated. "LOW-LEVEL WIND SHEAR.] Retrieved on 2007-11-25".
- [72] International Electrotechnical Commission: Sound level meters. IEC 61672-1 (2002)
- [73] International Organization for Standardization: Acoustics Procedure for describing aircraft noise heard on the ground. ISO 3891 (1978). [This standard may be replaced or supplemented by a new standard that is currently in draft form as ISO/CD 20906 (2003): Unattended monitoring of aircraft sound in the vicinity of airports.]
- [74] International Organization for Standardization: Acoustics Description, measurement and assessment of environmental noise – Part 1: Basic quantities and assessment procedures. ISO 1996-1 (2001).
- [75] International Civil Aviation Organization: International Standards and Recommended Practices, Environmental Protection, Annex 16, Volume I, Aircraft Noise, 4th Edition, July 2005.